



FOUNDATIONS

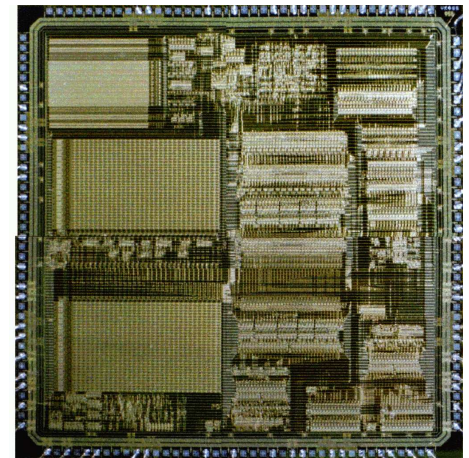
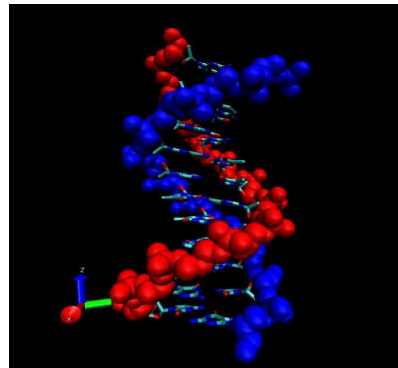
of

(LINEAR) SYSTEM THEORY

Jan C. Willems

K.U. Leuven, Flanders, Belgium

Systems



Features

- **open**
- **interconnected**
- **modular**
- **dynamic**

Features

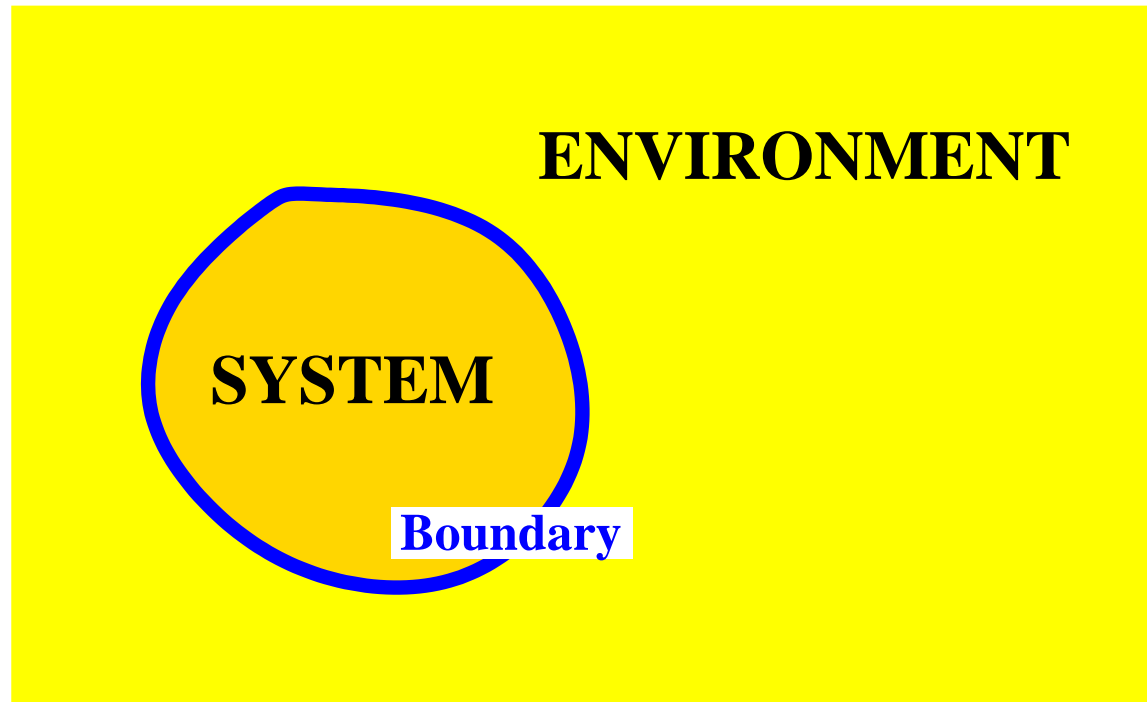
- **open**
- **interconnected**
- **modular**
- **dynamic**

Theme of this seminar:

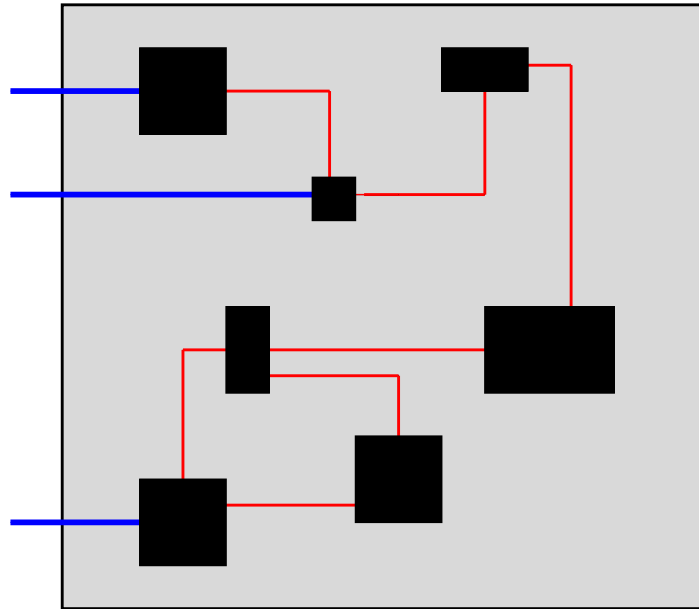
develop a suitable mathematical framework

Open and Connected

Open



Connected

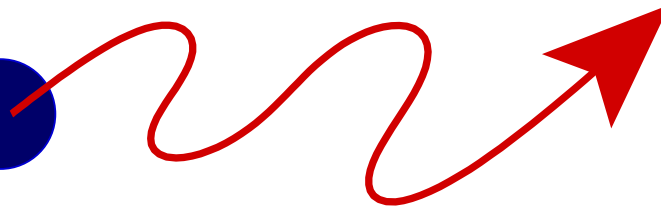
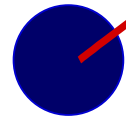


Architecture with subsystems

Historical introduction

How it all began ...

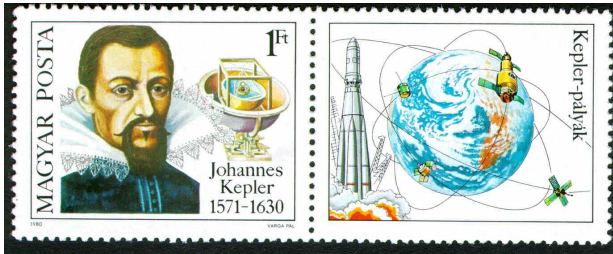
Planet



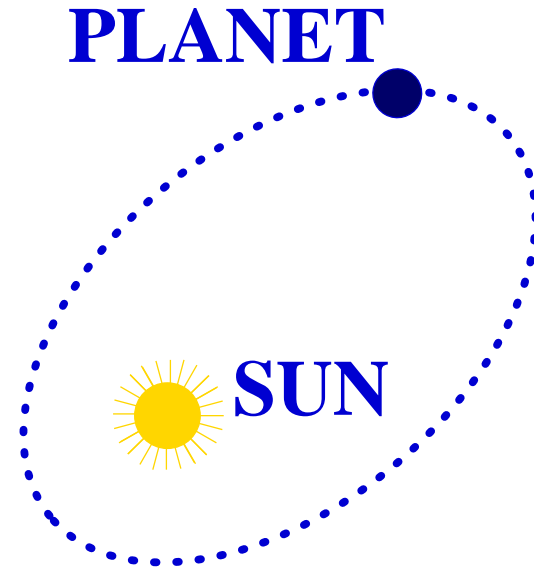
???

How, for heaven's sake, does it move?

Kepler's laws



Johannes Kepler (1571-1630)



Kepler's laws:

**Ellipse, sun in focus; = areas in = times;
(period)² \cong (diameter)³**

The equation of the planet

Consequence:

acceleration = function of position and velocity

$$\frac{d^2}{dt^2}w(t) = A\left(w(t), \frac{d}{dt}w(t)\right)$$

~> via **calculus** and **calculation**

$$\frac{d^2}{dt^2}w(t) + \frac{1}{|w(t)|^2} = 0$$



Isaac Newton (1643-1727)

The equation of the planet

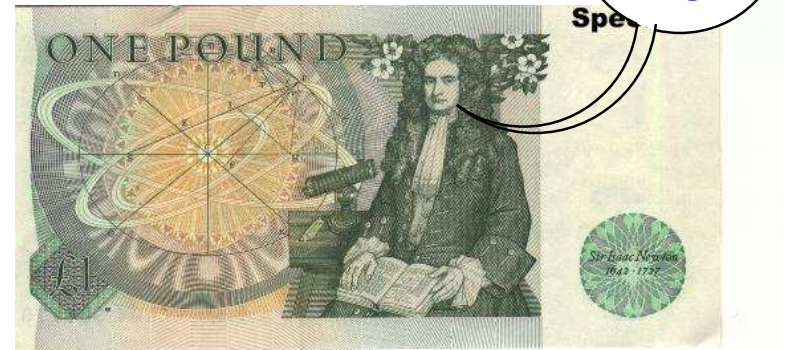
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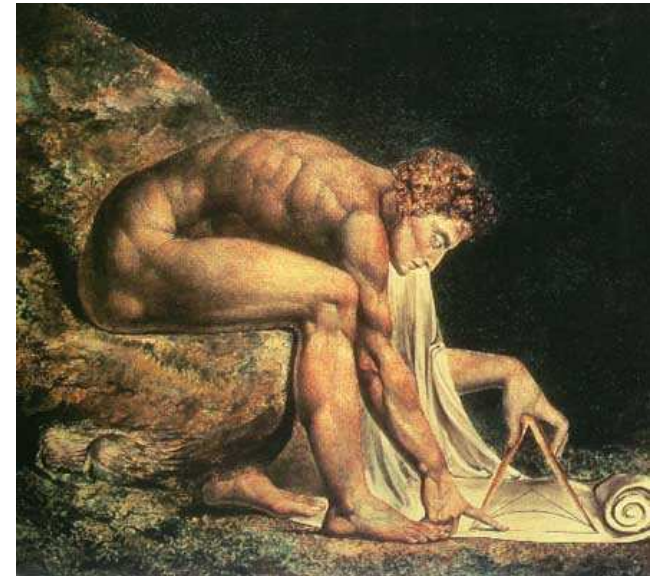
Newton's laws

tearing, zooming, linking

2-nd law $F'(t) = m \frac{d^2}{dt^2} w(t)$

gravity $F''(t) = m \frac{1_{w(t)}}{|w(t)|^2}$

3-rd law $F'(t) + F''(t) = 0$



$$\frac{d^2}{dt^2} w(t) + \frac{1_{w(t)}}{|w(t)|^2} = 0$$

The paradigm of *closed* systems

'Axiomatization'

K.1, K.2, & K.3

$$\rightsquigarrow \frac{d^2}{dt^2} w(t) + \frac{1_{w(t)}}{\left| \frac{d}{dt} w(t) \right|^2} = 0$$

$$\rightsquigarrow \frac{d}{dt} x = f(x)$$

\rightsquigarrow 'dynamical systems', flows

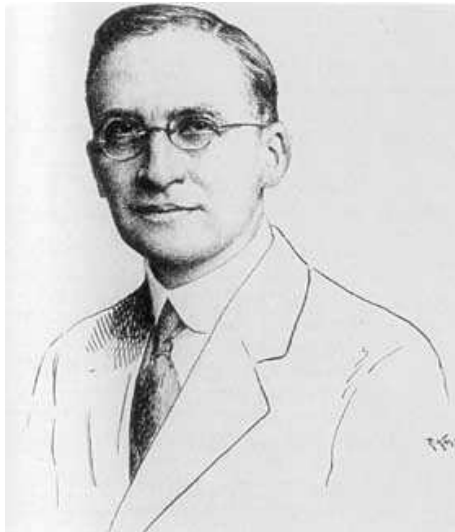
\rightsquigarrow **flows as paradigm of dynamics:** closed systems

Motion determined by internal initial conditions.

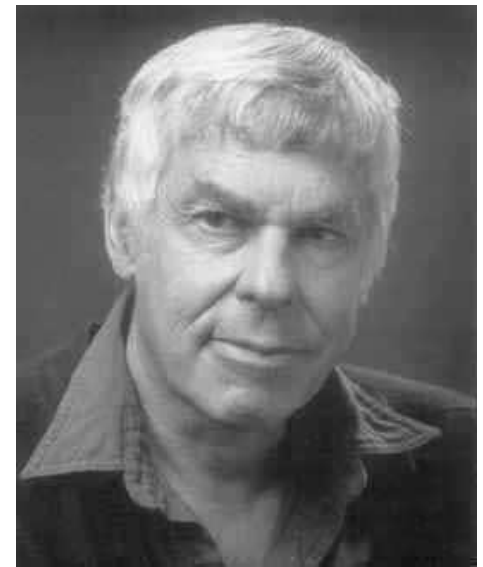
'Axiomatization'



Henri Poincaré (1854-1912)



George Birkhoff (1884-1944)



Stephen Smale (1930-)

'Axiomatization'

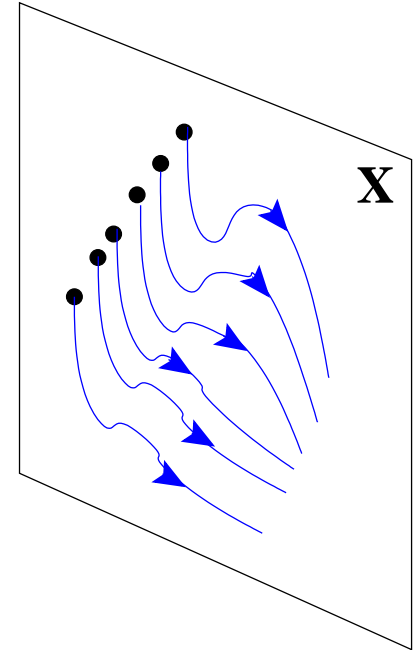
A *dynamical system* is defined by

a **state space** X and

a **state transition function**

$\phi : \dots$ such that \dots

$\phi(t, \mathbf{x}) =$ state at time t starting from state \mathbf{x}



This framework of **closed** systems

is **universally** used for dynamics

in mathematics and physics

'Axiomatization'

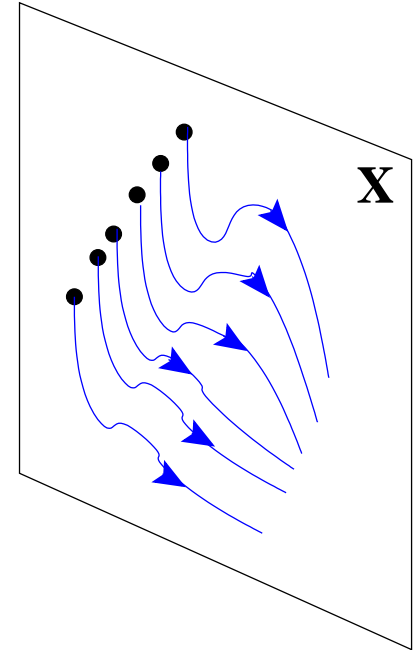
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How could they forget Newton's 2nd law,

about Maxwell's eq'ns,

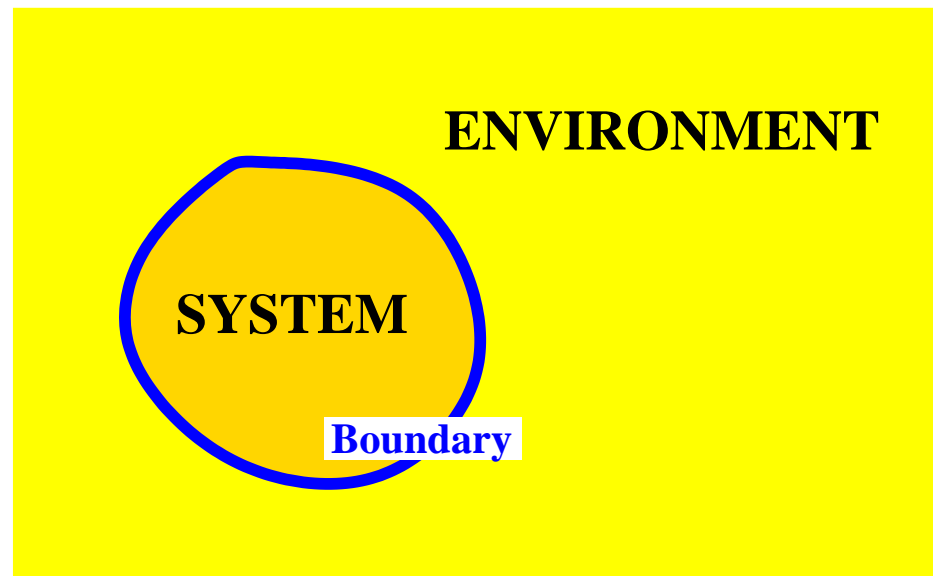
about thermodynamics,

about interconnection,

about tearing & zooming & linking, ...?

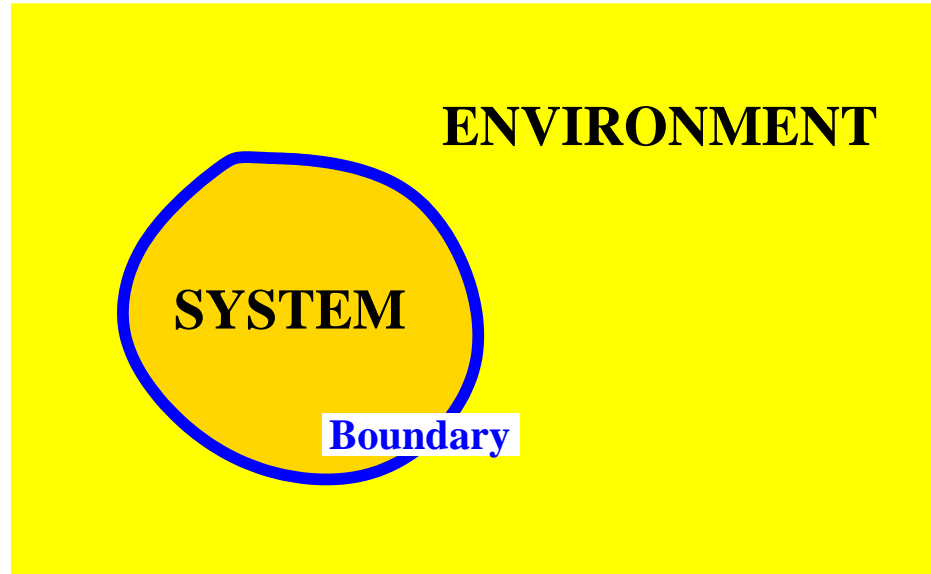
'Axiomatization'

Reply: assume 'fixed boundary conditions'



~> to model a system,
we have to model also the environment!

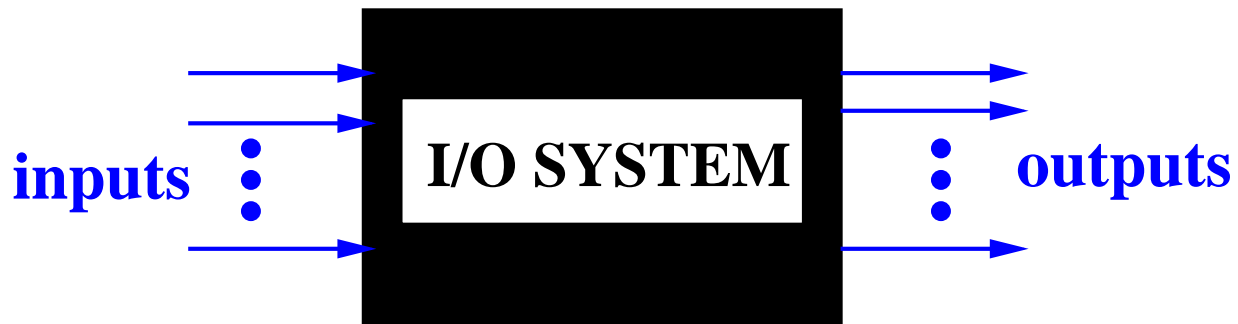
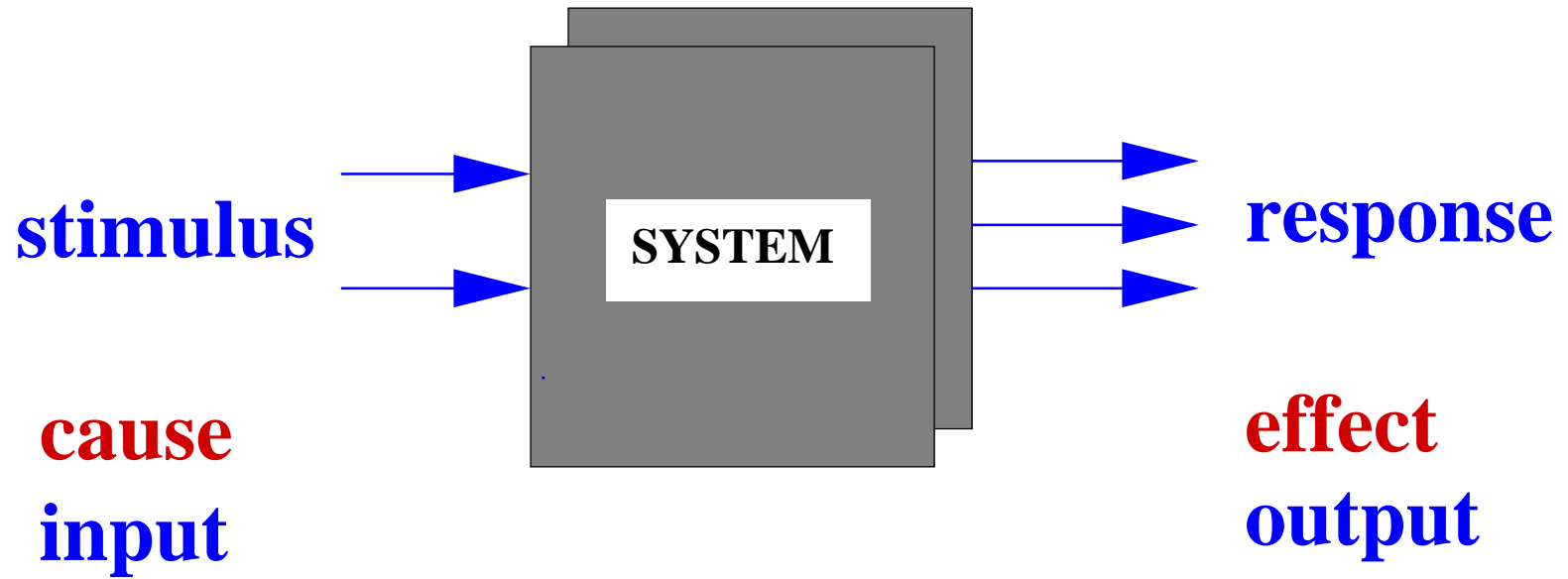
'Axiomatization'



**Chaos theory, cellular automata, sync, etc.,
function in this framework ...**

Meanwhile, in engineering, ...

Input/output systems



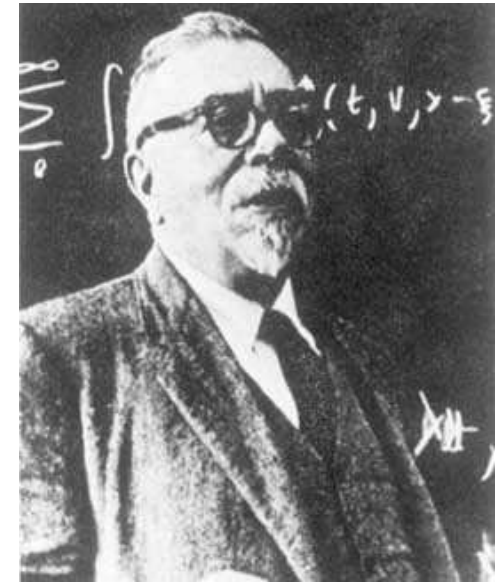
The originators



Lord Rayleigh (1842-1919)



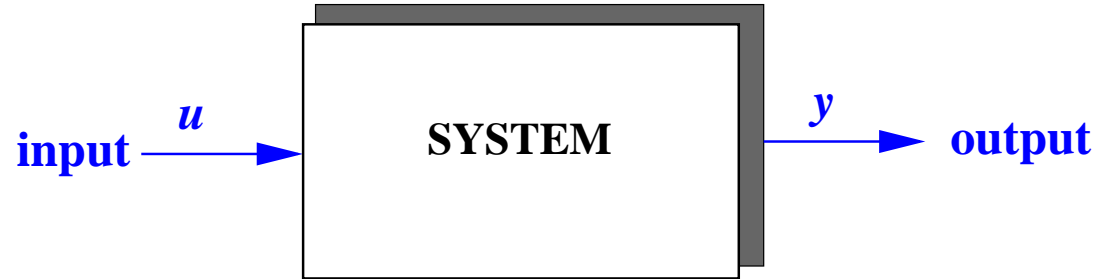
Oliver Heaviside (1850-1925)



Norbert Wiener (1894-1964)

and the many electrical circuit theorists ...

Mathematical description



Classical control

$$p \left(\frac{d}{dt} \right) y = q \left(\frac{d}{dt} \right) u$$

u : input, y : output, p and q polynomials

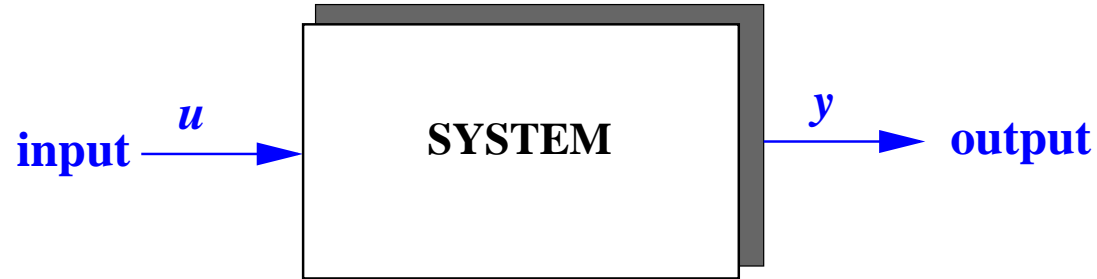
$G(s) = \frac{q(s)}{p(s)}$ transfer functions, impedances, admittances.

PID rules. Bode, Nyquist, Nichols. Lead-lag. Root-locus.

Mathematical framework:

Laplace t'fms, instead of symbolic calculus

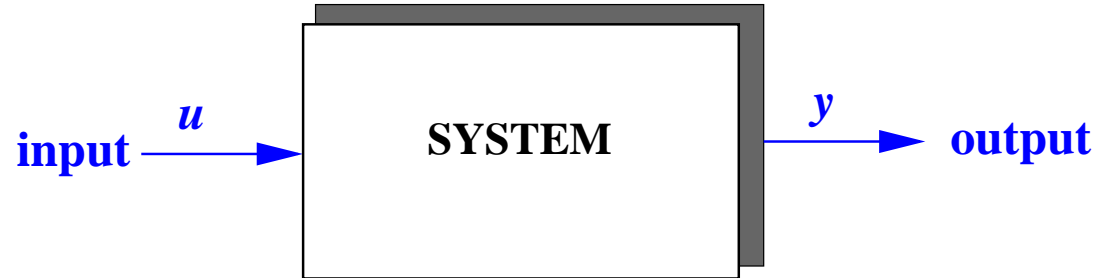
Mathematical description



$$y(t) = \int_{0 \text{ or } -\infty}^t H(t - t') u(t') dt'$$

$$y(t) = H_0(t) + \int_{-\infty}^t H_1(t - t') u(t') dt' + \\ \int_{-\infty}^t \int_{-\infty}^{t'} H_2(t - t', t' - t'') u(t') u(t'') dt' dt'' + \dots$$

Mathematical description



$$y(t) = \int_{0 \text{ or } -\infty}^t H(t - t') u(t') dt'$$

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Far from the physics

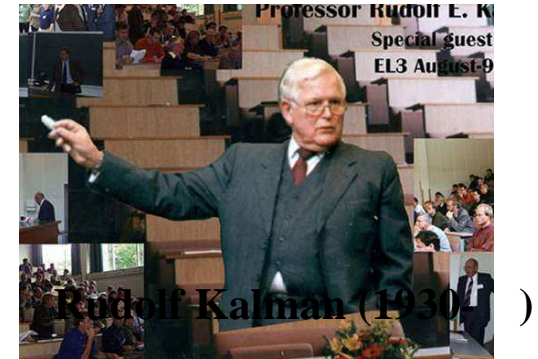
Fail to deal with **'initial conditions'**.

A system is **seldom** an i/o map

Input/state/output systems

Around 1960: a **paradigm shift** to

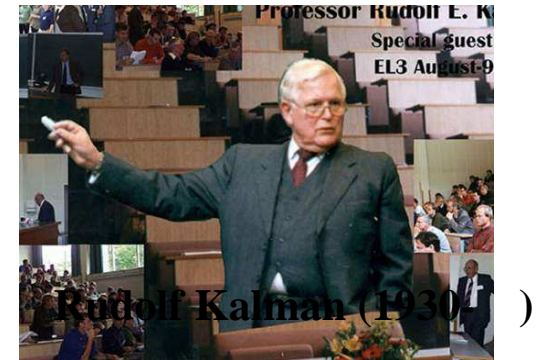
$$\frac{d}{dt}\mathbf{x} = f(\mathbf{x}, \mathbf{u}), \quad \mathbf{y} = g(\mathbf{x}, \mathbf{u})$$



Input/state/output systems

Around 1960: a **paradigm shift** to

$$\frac{d}{dt}\mathbf{x} = \mathbf{f}(\mathbf{x}, \mathbf{u}), \quad \mathbf{y} = \mathbf{g}(\mathbf{x}, \mathbf{u})$$



1. open, flows special case
2. ready to be interconnected
outputs of one system \mapsto inputs of another
3. deals with initial conditions
4. incorporates nonlinearities, time-variation
5. models many physical phenomena
6. ...

Input/state/output systems

The **input/state/output** view turned out to be very effective and fruitful

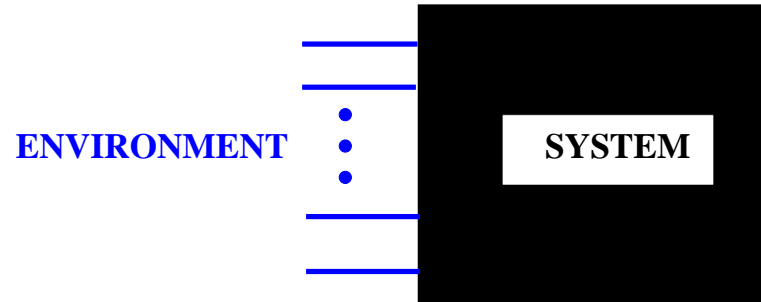
- for **modeling**
- for **control** (stabilization, robustness, ...)

Input/state/output systems

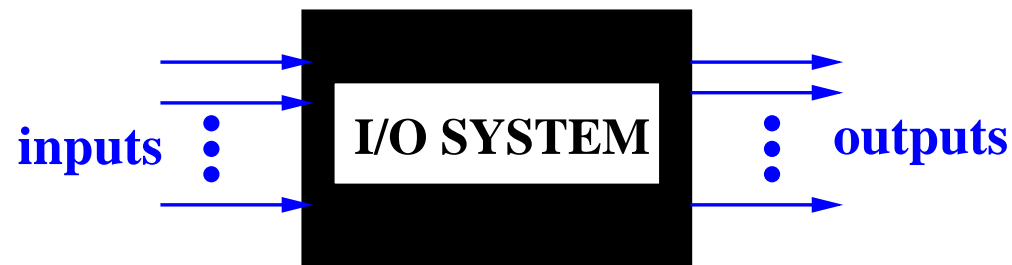
The **input/state/output** view turned out to be very effective and fruitful

- for **modeling**
- for **control** (stabilization, robustness, ...)
- **prediction** of one signal from another, **filtering**
- understanding **system representations**
(transfer f'n, input/state/output, etc.)
- model simplification, **reduction**
- **system ID:** models from data
- etc., etc., etc.

Open and Connected

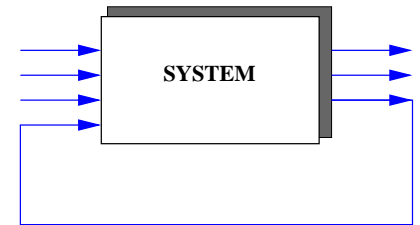
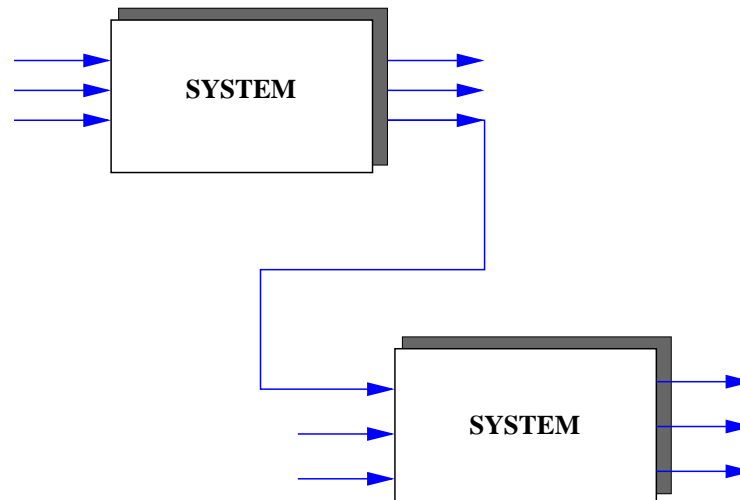
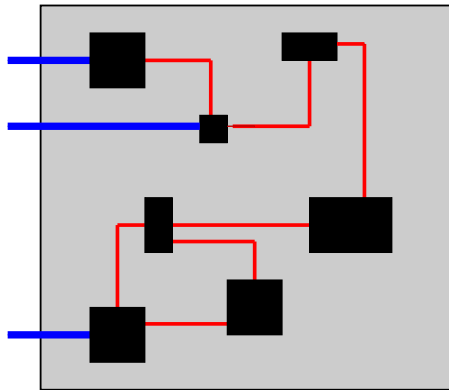


In system theory, we are accustomed to view an open dynamical system as an **input/output structure**



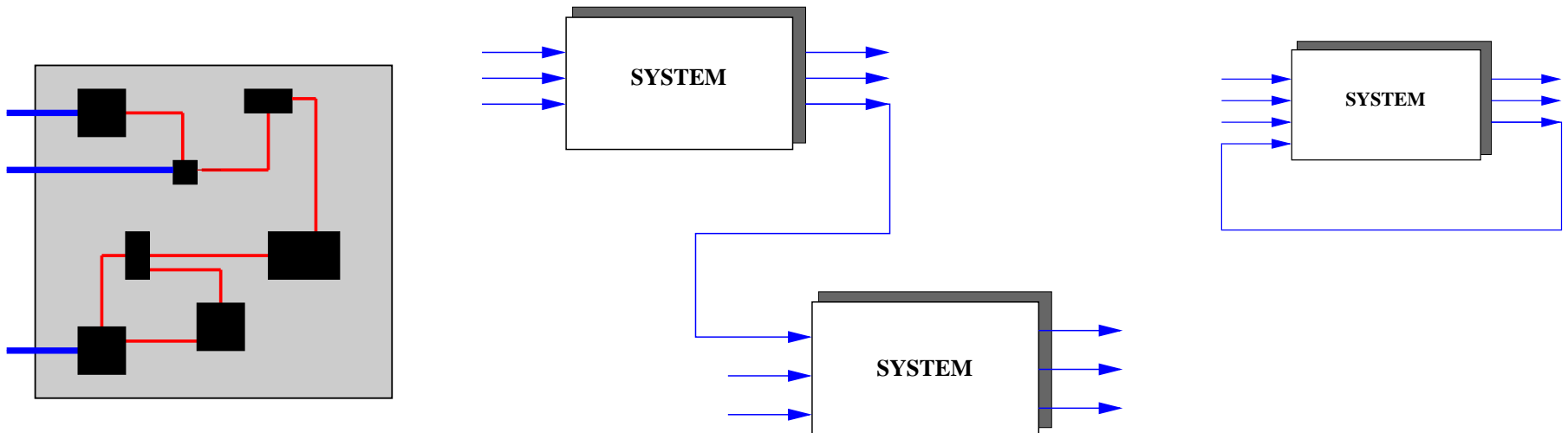
Open and Connected

In system theory, we are accustomed to view an open dynamical system as an **input/output structure** & interconnection as **output-to-input assignment**.



Open and Connected

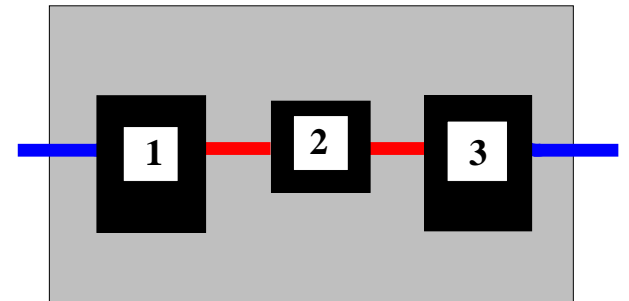
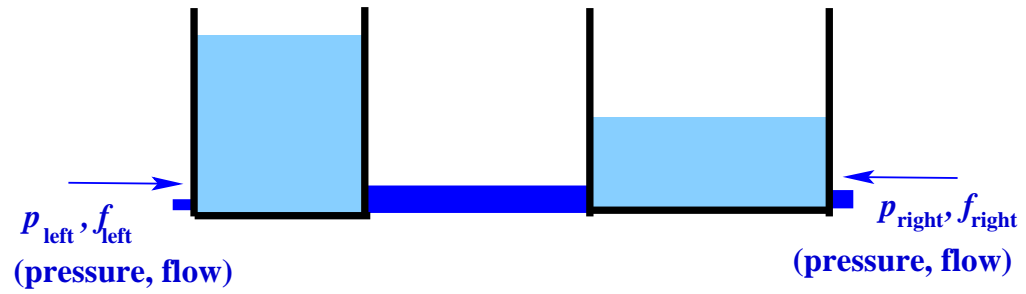
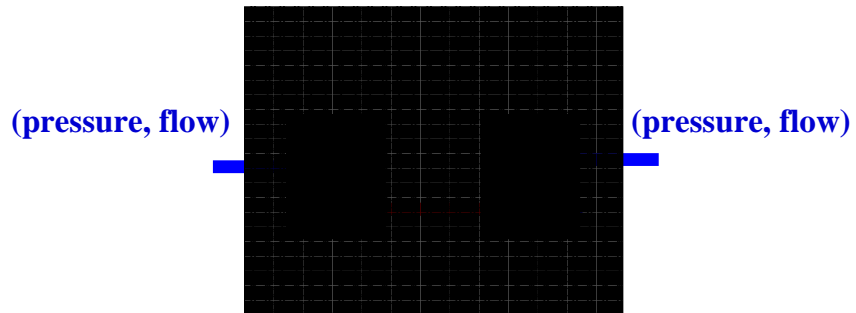
In system theory, we are accustomed to view an open dynamical system as an **input/output structure** & interconnection as **output-to-input assignment**.



Is this appropriate for modeling **physical** systems?

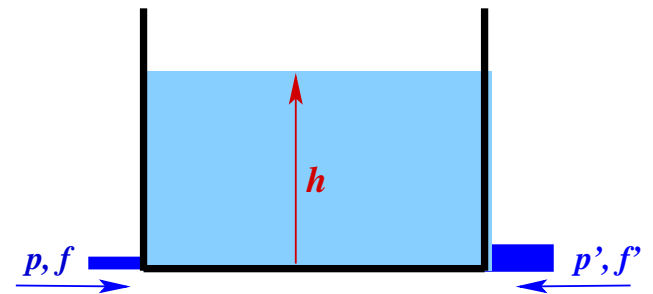
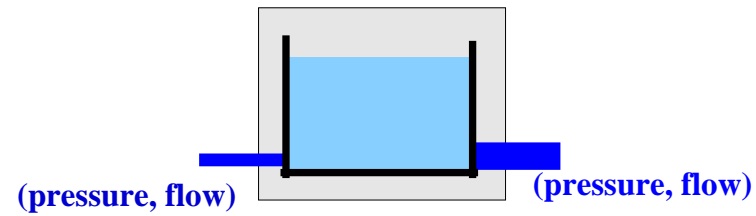
Interconnection in physical systems

Example



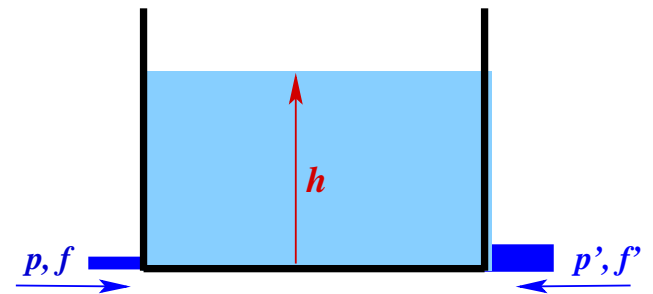
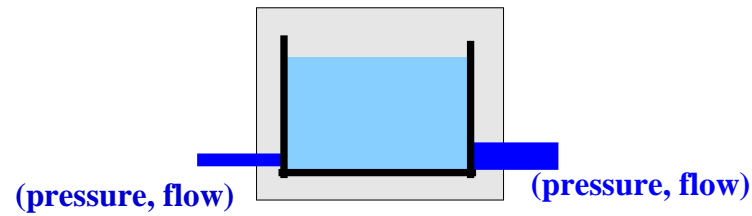
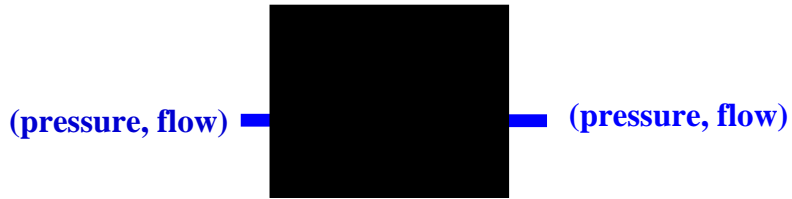
Example

Subsystems 1 and 3:



Example

Subsystems 1 and 3:



Subsystem 2:



Example

Interconnection laws:



$$p = p', \quad f + f' = 0.$$

$$\begin{aligned}
A_1 \frac{d}{dt} h_1 &= f_1 + f'_1, \\
B_1 f_1 &= \begin{cases} \sqrt{|p_1 - p_0 - \rho h_1|} & \text{if } p_1 - p_0 \geq \rho h_1, \\ -\sqrt{|p_1 - p_0 - \rho h_1|} & \text{if } p_1 - p_0 \leq \rho h_1, \end{cases} \\
C f'_1 &= \begin{cases} \sqrt{|p'_1 - p_0 - \rho h_1|} & \text{if } p'_1 - p_0 \geq \rho h_1, \\ -\sqrt{|p'_1 - p_0 - \rho h_1|} & \text{if } p'_1 - p_0 \leq \rho h_1, \end{cases}
\end{aligned} \tag{1}$$

$$f_2 = -f'_2, \quad p_2 - p'_2 = \alpha f_2, \tag{2}$$

$$\begin{aligned}
A_3 \frac{d}{dt} h_3 &= f_3 + f'_3, \\
C f_3 &= \begin{cases} \sqrt{|p_3 - p_0 - \rho h_3|} & \text{if } p_3 - p_0 \geq \rho h_3, \\ -\sqrt{|p_3 - p_0 - \rho h_3|} & \text{if } p_3 - p_0 \leq \rho h_3, \end{cases} \\
C_3 f'_3 &= \begin{cases} \sqrt{|p'_3 - p_0 - \rho h_3|} & \text{if } p'_3 - p_0 \geq \rho h_3, \\ -\sqrt{|p'_3 - p_0 - \rho h_3|} & \text{if } p'_3 - p_0 \leq \rho h_3, \end{cases}
\end{aligned} \tag{3}$$

$$p'_1 = p_2, \quad f'_1 + f_2 = 0, \quad p'_2 = p_3, \quad f'_2 + f_3 = 0. \tag{4}$$

$$p_{\text{left}} = p_1, \quad f_{\text{left}} = f_1, \quad p_{\text{right}} = p'_3, \quad f_{\text{right}} = f'_3. \tag{5}$$

- **Unclear input/output structure for terminal variables**
- **Many variables, indivisibly, at the same terminal**
- **Interconnection = variable sharing**
- **No signal flows, no output-to-input assignment**
- **...**

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- **...**

“Block diagrams unsuitable for serious physical modeling

- the control/physics barrier”

“Behavior based (declarative) modeling is a good alternative”



from K.J. Åström, *Present Developments in Control Applications*



**IFAC 50-th Anniversary Celebration
Heidelberg, September 12, 2006.**

Behavioral systems

A dynamical system

$:\Leftrightarrow$ a family of time functions, *'the behavior'*

Interconnection $:\Leftrightarrow$ *'variable sharing'*.

Control $:\Leftrightarrow$ *interconnection*.

Modeling of interconnected physical systems is the strongest case for 'behaviors'.

Models

A dynamical system : $\Leftrightarrow (\mathbb{T}, \mathbb{W}, \mathfrak{B})$

$\mathbb{T} \subseteq \mathbb{R}$ ‘time set’

\mathbb{W} ‘signal space’

$\mathfrak{B} \subseteq \mathbb{W}^{\mathbb{T}}$ the ‘behavior’

a family of trajectories $\mathbb{T} \rightarrow \mathbb{W}$

mostly, today, $\mathbb{T} = \mathbb{R}, \mathbb{W} = \mathbb{R}^w$, hence \mathfrak{B} is a family of vector-valued continuous-time trajectories

$w : \mathbb{R} \rightarrow \mathbb{R}^w \in \mathfrak{B}$: ‘ w is compatible with the model’

$w : \mathbb{R} \rightarrow \mathbb{R}^w \notin \mathfrak{B}$: ‘the model forbids w ’

Models

The dynamical system $(\mathbb{R}, \mathbb{R}^w, \mathfrak{B}) \rightsquigarrow \mathfrak{B}$

linear $:\Leftrightarrow w_1, w_2 \in \mathfrak{B}, \alpha \in \mathbb{R}$

$\Rightarrow \alpha w_1 + w_2 \in \mathfrak{B}$

time-invariant $:\Leftrightarrow w \in \mathfrak{B}, \sigma$ any shift,

$\Rightarrow \sigma w \in \mathfrak{B}$

differential $:\Leftrightarrow$ ‘described’ by an ODE.

Models

For example,

$$\frac{d}{dt}x = Ax + Bu, y = Cx + Du, \quad w = \begin{bmatrix} u \\ y \\ x \end{bmatrix} \quad \text{or } w = \begin{bmatrix} u \\ y \end{bmatrix}$$

DAE's $F \frac{d}{dt}x + Gx + Hw = 0$

$$P \left(\frac{d}{dt} \right) y = Q \left(\frac{d}{dt} \right) u, \quad w = \begin{bmatrix} u \\ y \end{bmatrix}, \quad P, Q \text{ polynomial matrices}$$

$$y = G \left(\frac{d}{dt} \right) u, \quad w = \begin{bmatrix} u \\ y \end{bmatrix}, \quad G \text{ matrix of rational f'ns}$$

etc., and their nonlinear analogues

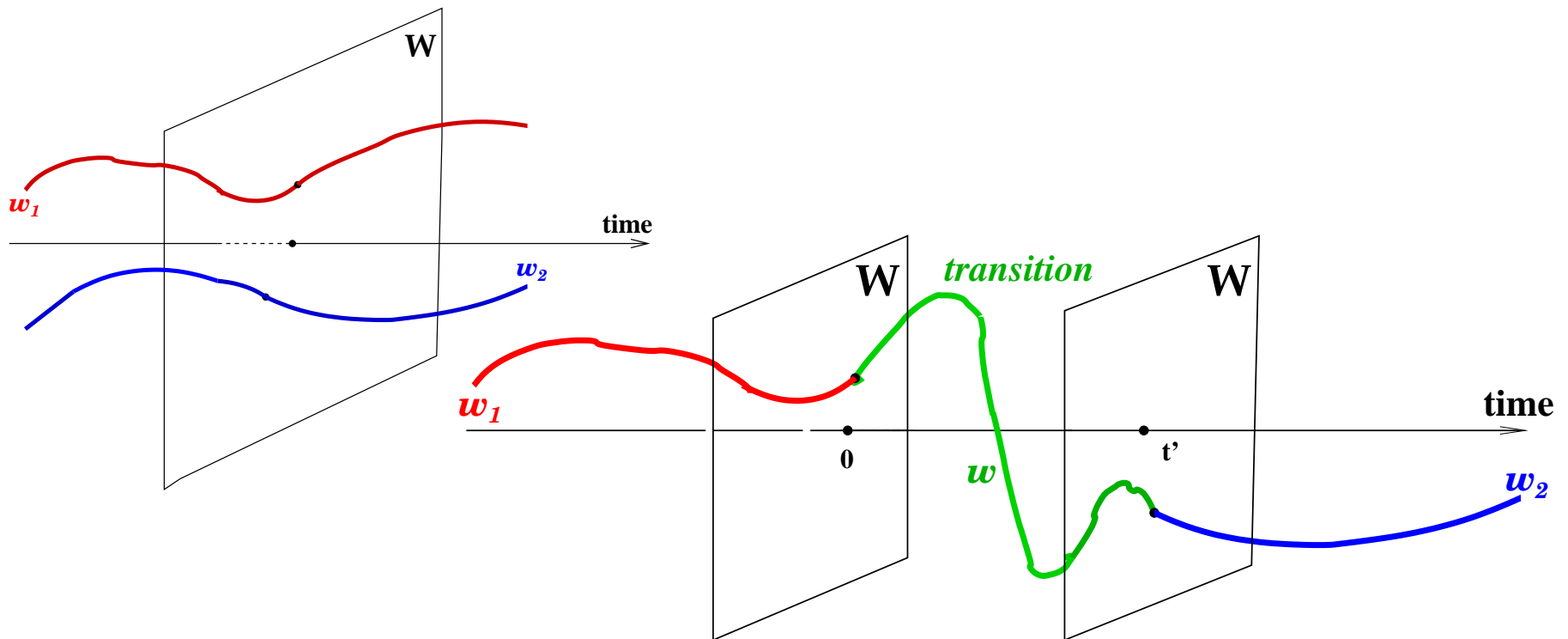
Controllability as a system property

Controllability

The time-invariant system $(\mathbb{R}, \mathbb{R}^w, \mathfrak{B})$ is

controllable $:\Leftrightarrow$

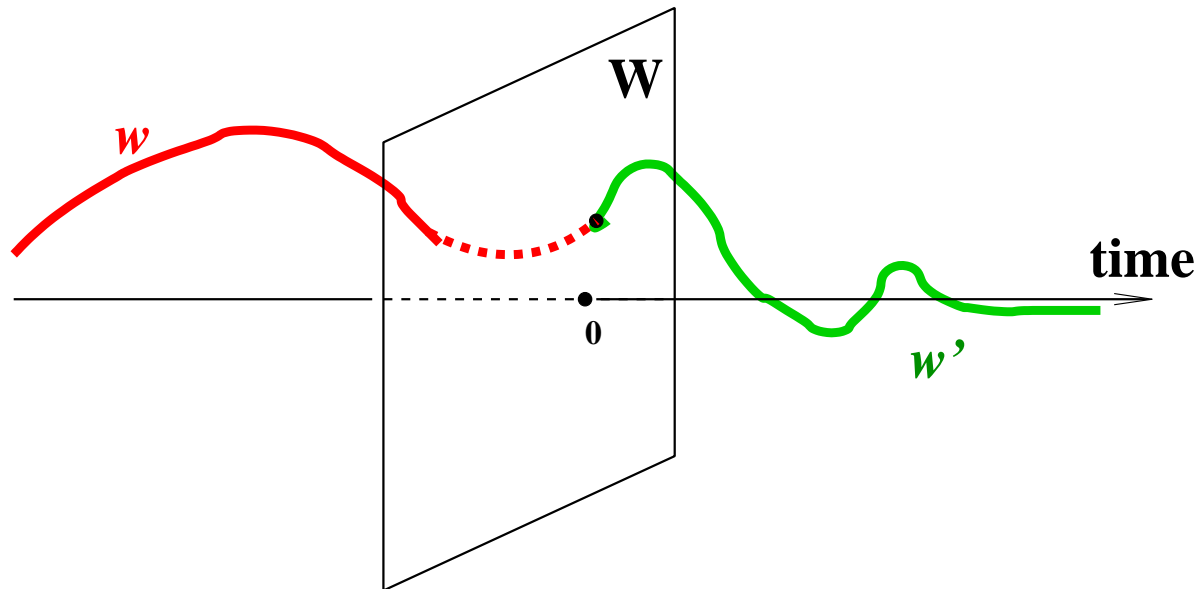
$\forall w_1, w_2 \in \mathfrak{B}, \exists w \in \mathfrak{B}$ and $T \geq 0$ such that



Controllability

The time-invariant system $(\mathbb{R}, \mathbb{R}^w, \mathcal{B})$ is

stabilizable $:\Leftrightarrow \forall w \in \mathcal{B}, \exists w' \in \mathcal{B}$ such that



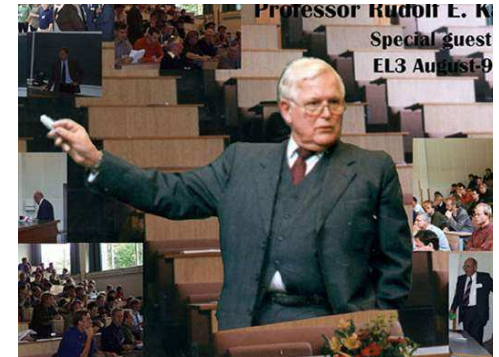
Controllability

Makes controllability into a bona fide, genuine, true system property, instead of of merely a (state space) representation.

State Controllability

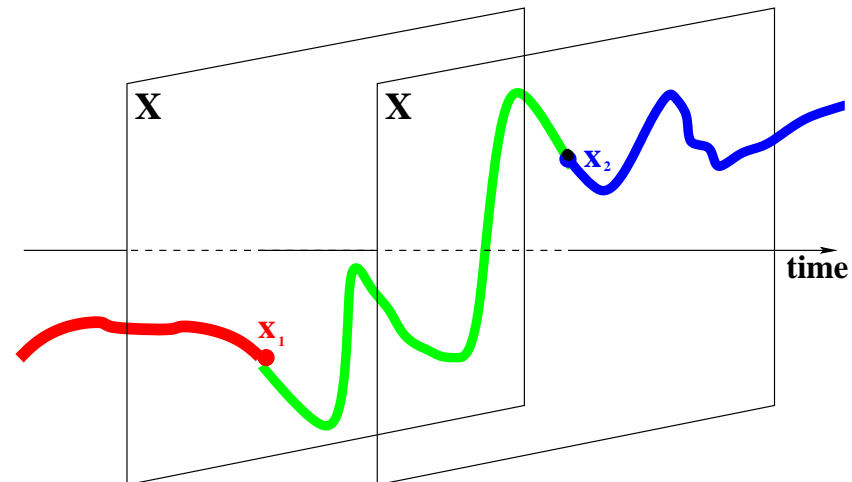
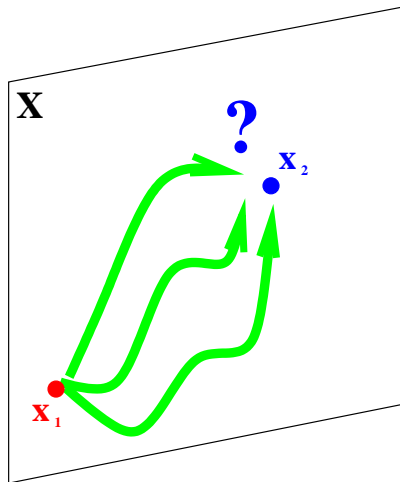
Special case: classical Kalman definitions for

$$\frac{d}{dt}x = f(x, u).$$



controllability: variables = state or (input, state)

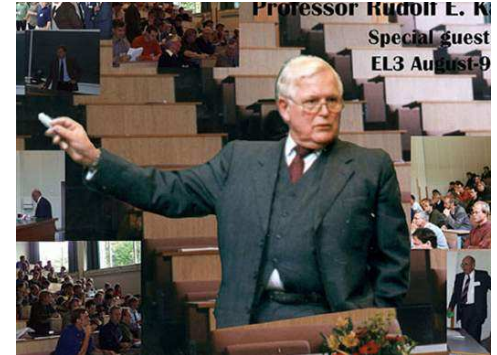
This is a **special case** of our controllability:



State Controllability

Special case: classical Kalman definitions for

$$\frac{d}{dt}x = f(x, u).$$



controllability: variables = state or (input, state)

Why should we be so concerned with the state?

If a system is not (state) controllable, why is it?

Insufficient influence of the control?

Or bad choice of the state?

Or not properly editing the equations?

Kalman's definition addresses a rather special situation.

The basics of LTIDS

LTIDS

The dynamical system $(\mathbb{R}, \mathbb{R}^w, \mathfrak{B})$ is

linear, **time-invariant**, and **differential** (LTIDS)

$:\Leftrightarrow$ ‘described’ by an ODE

$$R_0 w + R_1 \frac{d}{dt} w + \cdots + R_n \frac{d^n}{dt^n} w = 0.$$

R_0, R_1, \cdots, R_n real matrices.

LTIDS

$$R_0 w + R_1 \frac{d}{dt} w + \cdots + R_n \frac{d^n}{dt^n} w = 0.$$

R_0, R_1, \dots, R_n real matrices.

$$\rightsquigarrow R \left(\frac{d}{dt} \right) w = 0$$

$R = R_0 + R_1 \xi + \cdots + R_n \xi^n$ polynomial matrix.

R typically 'wide'



LTIDS

$$R_0 w + R_1 \frac{d}{dt} w + \cdots + R_n \frac{d^n}{dt^n} w = 0.$$

R_0, R_1, \dots, R_n real matrices.

$$\rightsquigarrow R \left(\frac{d}{dt} \right) w = 0$$

$R = R_0 + R_1 \xi + \cdots + R_n \xi^n$ polynomial matrix.

Defines $\mathfrak{B} = \text{kernel} \left(R \left(\frac{d}{dt} \right) \right)$ ‘kernel representation’

Notation: $\mathfrak{L}^w, \mathfrak{L}^\bullet$.

\mathcal{L}^w as a module

Let $\mathfrak{B} = \text{kernel} \left(R \left(\frac{d}{dt} \right) \right)$

R determines \mathfrak{B} , but \mathfrak{B} does not determine R !

What is the mathematical structure of \mathcal{L}^w ?

\mathcal{L}^w as a module

Consider $\mathfrak{B} \in \mathcal{L}^w$. Call $n \in \mathbb{R}[\xi]^w$ an **annihilator**

$:\Leftrightarrow$

$$n \left(\frac{d}{dt} \right) w = 0 \text{ for all } w \in \mathfrak{B}$$

Examples:

Transposes of rows of R

for $\mathfrak{B} = \text{kernel} \left(R \left(\frac{d}{dt} \right) \right)$

\mathcal{L}^w as a module

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Note

- n_1, n_2 annihilators $\Rightarrow n_1 + n_2$ annihilator
- n annihilator, p polynomial $\Rightarrow pn$ annihilator

\Rightarrow Annihilators of \mathfrak{B} form a submodule of $\mathbb{R} [\xi]^w$.

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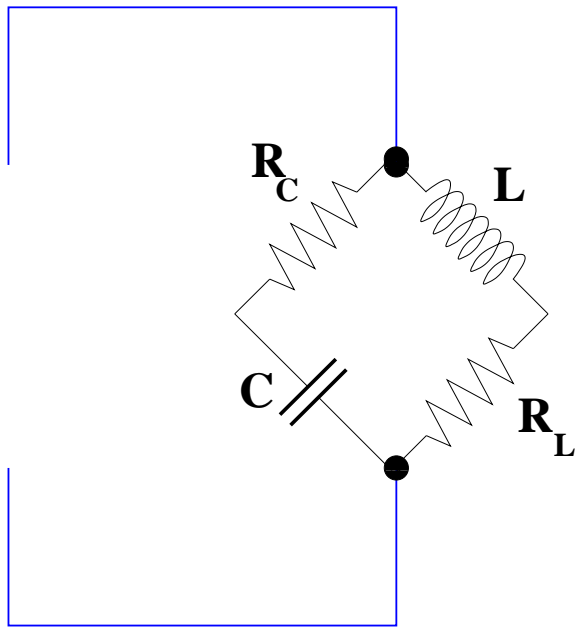
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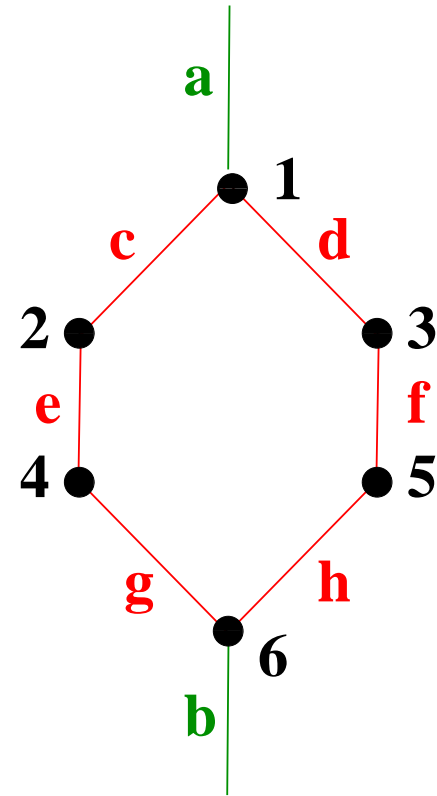
Thm. 1: \exists 1 \leftrightarrow 1 relation between \mathcal{L}^w and submodules of $\mathbb{R} [\xi]^w$

Elimination

Motivating example: model port behavior of



(a)



(b)

by tearing, zooming, and linking

Elimination

Module equations

vertex 1 : $V_{\text{connector}_{1,1}} = V_{\text{connector}_{1,2}} = V_{\text{connector}_{1,3}}$
 $I_{\text{connector}_{1,1}} + I_{\text{connector}_{1,2}} + I_{\text{connector}_{1,3}} = 0$

vertex 2 : $V_{R_C,1} - V_{R_C,2} = R_C I_{R_C,1}, I_{R_C,1} + I_{R_C,2} = 0$

vertex 3 : $L \frac{d}{dt} I_{L,1} = V_{L,1} - V_{L,2}, I_{L,1} + I_{L,2} = 0$

vertex 4 : $C \frac{d}{dt} (V_{C,1} - V_{C,2}) = I_{C,1}, I_{C,1} + I_{C,2} = 0$

vertex 5 : $V_{R_L,1} - V_{R_L,2} = R_L I_{R_L,1}$
 $I_{R_L,1} + I_{R_L,2} = 0$

vertex 6 : $V_{\text{connector}_{2,1}} = V_{\text{connector}_{2,2}} = V_{\text{connector}_{2,3}}$
 $I_{\text{connector}_{2,1}} + I_{\text{connector}_{2,2}} + I_{\text{connector}_{2,3}} = 0$

Elimination

Interconnection equations

$$\text{edge c : } V_{RC,1} = V_{\text{connector}12} I_{RC,1} + I_{\text{connector}1,2} = 0$$

$$\text{edge d : } V_{L1} = V_{\text{connector}13} I_{L1} + I_{\text{connector}13} = 0$$

$$\text{edge e : } V_{RC,2} = V_{C1} I_{RC,2} + I_{C1} = 0$$

$$\text{edge f : } V_{L2} = V_{RC,1} I_{L2} + I_{RL,1} = 0$$

$$\text{edge g : } V_{C2} = V_{\text{connector}21} I_{C2} + I_{\text{connector}21} = 0$$

$$\text{edge h : } V_{RL,2} = V_{\text{connector}22} I_{RL,2} + I_{\text{connector}22} = 0$$

Elimination

Manifest variable assignment

$$V_{\text{externalport}} = V_{\text{connector}_{1,1}} - V_{\text{connector}_{2,3}}$$

$$I_{\text{externalport}} = I_{\text{connector}_{1,1}}$$

Elimination

Manifest variable assignment

$$V_{\text{externalport}} = V_{\text{connector}_{1,1}} - V_{\text{connector}_{2,3}}$$

$$I_{\text{externalport}} = I_{\text{connector}_{1,1}}$$

What equation(s) governs the behavior of

$$(V_{\text{externalport}}, I_{\text{externalport}})$$

Constant-coefficient linear differential equation?

Elimination

$\rightsquigarrow \Sigma = (\mathbb{R}, \mathbb{R}^2, \mathfrak{B})$ behavior \mathfrak{B} specified by:

Case 1: $CR_C \neq \frac{L}{R_L}$

$$\begin{aligned} \left(\frac{R_C}{R_L} + \left(1 + \frac{R_C}{R_L} \right) CR_C \frac{d}{dt} + CR_C \frac{L}{R_L} \frac{d^2}{dt^2} \right) V_{\text{externalport}} \\ = \left(1 + CR_C \frac{d}{dt} \right) \left(1 + \frac{L}{R_L} \frac{d}{dt} \right) R_C I_{\text{externalport}} \end{aligned}$$

Case 2: $CR_C = \frac{L}{R_L}$

$$\left(\frac{R_C}{R_L} + CR_C \frac{d}{dt} \right) V_{\text{externalport}} = (1 + CR_C) \frac{d}{dt} R_C I_{\text{externalport}}$$

Elimination Theorem

Thm. 2: \mathcal{L}^\bullet is closed under projection

Elimination Theorem

Thm. 2: \mathcal{L}^\bullet is closed under projection

Consider

$$R_1 \left(\frac{d}{dt} \right) w_1 + R_2 \left(\frac{d}{dt} \right) w_2 = 0 \rightsquigarrow \text{behavior } \mathfrak{B}$$

Define

$$\mathfrak{B}_1 := \{w_1 \mid \exists w_2 \text{ such that } (w_1, w_2) \in \mathfrak{B}\}$$

Elimination thm $\Rightarrow \exists R$ such that $\mathfrak{B}_1 = \text{kernel} \left(R \left(\frac{d}{dt} \right) \right)!$

E.g. $\frac{d}{dt}x = Ax + Bu, y = Cx + Du \Rightarrow P\left(\frac{d}{dt}\right)y = Q\left(\frac{d}{dt}\right)u$
linear DAE's allow elimination of nuisance variables

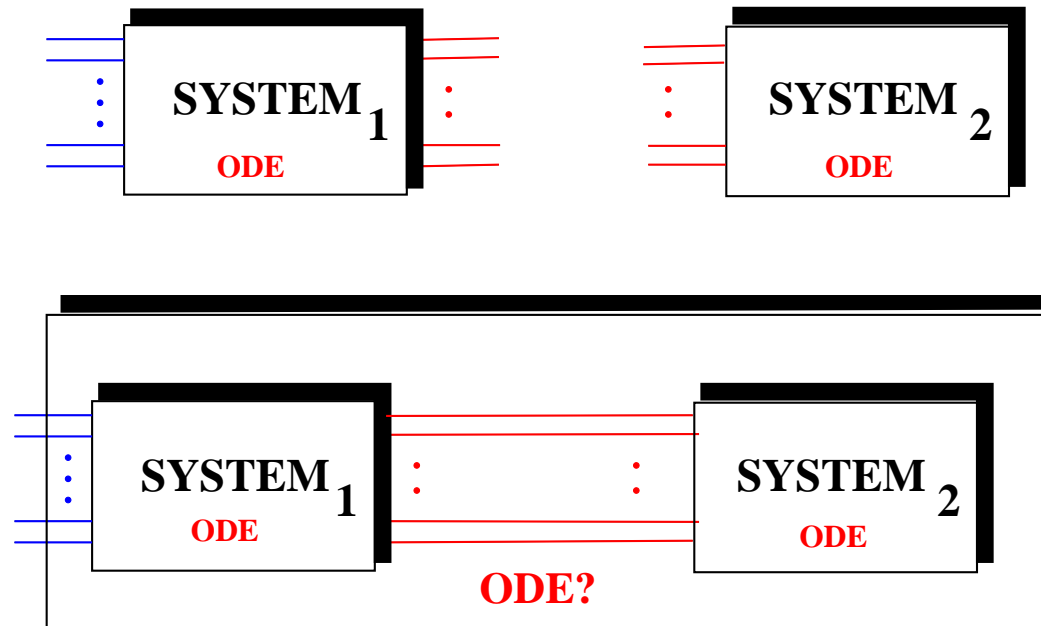
Elimination Theorem

Thm. 2: \mathcal{L}^\bullet is closed under projection

\mathcal{L}^\bullet is closed under intersection, addition, projection

Elimination Theorem

Thm. 2: \mathcal{L}° is closed under projection



**In LTIDS systems 1 and 2 ODEs \Rightarrow interconnection ODE.
In nonlinear case, very unlikely described by ODE, even if systems 1 and 2 are!**

Why are ODE models so common?

Image representation

$$w = M \left(\frac{d}{dt} \right) \ell \quad \rightsquigarrow w\text{-behavior } \mathfrak{B} = \text{image} \left(M \left(\frac{d}{dt} \right) \right)$$

Elimination thm $\Rightarrow \mathfrak{B} = \text{kernel} \left(R \left(\frac{d}{dt} \right) \right)$, for some R .

So, all images are kernels, but what kernels are images?

$\Leftrightarrow \mathfrak{B}$ is controllable

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So, all images are kernels, but what kernels are images?

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Thm. 3: $\mathfrak{B} \in \mathcal{L}^\bullet$ controllable \Leftrightarrow admits image representation

Leads to controllability tests.

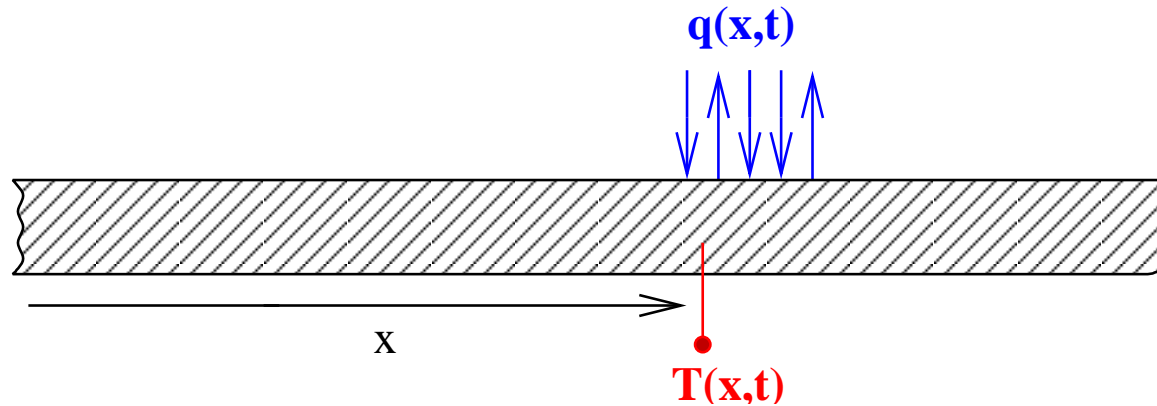
There are various other tests for controllability, e.g.

$$\text{rank} (R(\lambda)) \text{ the same } \forall \lambda \in \mathbb{C}$$

Partial differential equations

PDEs: Examples

Diffusion



$$\frac{\partial}{\partial t} T = \frac{\partial^2}{\partial x^2} T + q$$

independent variables: (t, x) time and space

dependent variables: (T, q) temperature and heat

PDEs: Examples

Wave phenomena

$$\frac{\partial^2 w}{\partial t^2} = \frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial y^2}$$

independent variables: (t, x, y) time and space

dependent variables: w deflection

PDEs: Examples

Maxwell's equations for EM fields in free space



$$\begin{aligned}\nabla \cdot \vec{E} &= \frac{1}{\epsilon_0} \rho, \\ \nabla \times \vec{E} &= -\frac{\partial}{\partial t} \vec{B}, \\ \nabla \cdot \vec{B} &= 0, \\ c^2 \nabla \times \vec{B} &= \frac{1}{\epsilon_0} \vec{j} + \frac{\partial}{\partial t} \vec{E}.\end{aligned}$$

independent variables: (t, x, y, z) time and space

dependent variables: $(\vec{E}, \vec{B}, \vec{j}, \rho)$

electric field, magnetic field, current density, charge density

PDEs: Notation

$\mathbb{R} [\xi_1, \dots, \xi_n]$: **polynomials, n indet., real coeff.**

$\mathbb{R} [\xi_1, \dots, \xi_n]^{\bullet \times w}$, $\mathbb{R} [\xi_1, \dots, \xi_n]^{\bullet \times \bullet}$ **matrices of ...**

PDEs: Notation

$$R \in \mathbb{R} [\xi_1, \dots, \xi_n]^{\bullet \times w} \rightsquigarrow R \left(\frac{\partial}{\partial x_1}, \dots, \frac{\partial}{\partial x_n} \right) w = 0$$

linear constant coefficient PDEs with
n independent variables, x_1, \dots, x_n
w dependent variables, w_1, \dots, w_w
rowdim(R) = number of equations

PDEs: Notation

$$R \in \mathbb{R} [\xi_1, \dots, \xi_n]^{\bullet \times w} \rightsquigarrow R \left(\frac{\partial}{\partial x_1}, \dots, \frac{\partial}{\partial x_n} \right) w = 0$$

Ex.: Diffusion eq'n $\frac{\partial}{\partial t} T = \frac{\partial^2}{\partial x^2} T + q$

2 indep. variables, (t, x) , $w = 2$, $w = (T, q)$, 1 eq'n.

$$R(\xi_t, \xi_x) = [\xi_t - \xi_x^2 \mid - 1]$$

PDEs: Notation

$$R \in \mathbb{R} [\xi_1, \dots, \xi_n]^{\bullet \times w} \rightsquigarrow R \left(\frac{\partial}{\partial x_1}, \dots, \frac{\partial}{\partial x_n} \right) w = 0$$

Example: Maxwell's eq'ns

4 independent variables, (t, x, y, z)

$w = 10$, $w = (\vec{E}, \vec{B}, \vec{j}, \rho)$

8 equations, R 8×10 , sparse, first order

PDEs: Notation

$$R \in \mathbb{R} [\xi_1, \dots, \xi_n]^{\bullet \times w} \rightsquigarrow R \left(\frac{\partial}{\partial x_1}, \dots, \frac{\partial}{\partial x_n} \right) w = 0$$

Behavior:

$$\mathfrak{B} = \{ w \in \mathcal{C}^\infty(\mathbb{R}^n, \mathbb{R}^w) \mid R \left(\frac{\partial}{\partial x_1}, \dots, \frac{\partial}{\partial x_n} \right) w = 0 \}$$

Notation:

$$\mathfrak{B} \in \mathcal{L}_n^w, \quad \mathfrak{B} = \text{kernel} \left(R \left(\frac{\partial}{\partial x_1}, \dots, \frac{\partial}{\partial x_n} \right) \right)$$

PDEs: Notation

$$R \in \mathbb{R} [\xi_1, \dots, \xi_n]^{\bullet \times w} \rightsquigarrow R \left(\frac{\partial}{\partial x_1}, \dots, \frac{\partial}{\partial x_n} \right) w = 0$$

Linear constant coefficient PDEs

C^∞ -solutions

infinite domain, no boundary conditions

‘everything’ valid for convex, open domain $\Omega \subseteq \mathbb{R}^n$

\mathcal{L}_n^w : the basics



Thm. 1:

$\mathcal{L}_n^w \iff$ the submodules of $\mathbb{R} [\xi_1, \dots, \xi_n]^w$

Thm. 2: Elimination thm

\mathcal{L}_n^w is closed under projection

Thm. 3:

$\mathcal{B} \in \mathcal{L}_n^w$ is controllable $\iff \mathcal{B}$ is an image

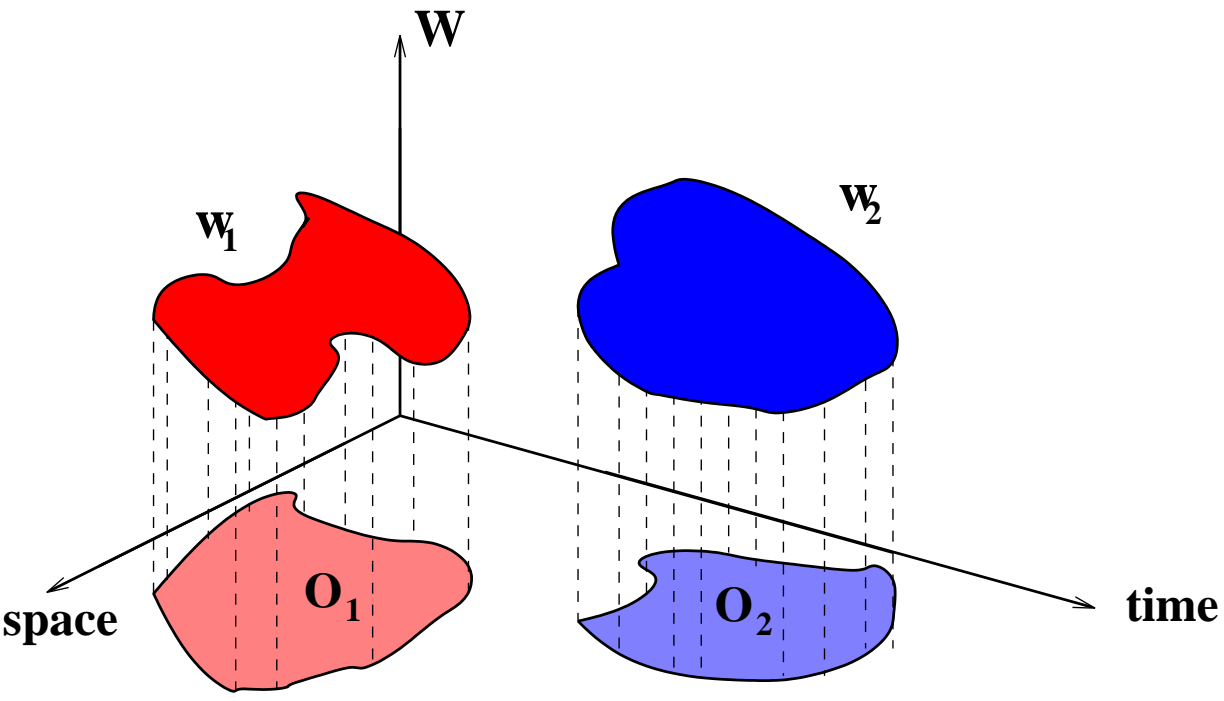


Describe (ρ, \vec{E}, \vec{j}) in Maxwell's equations

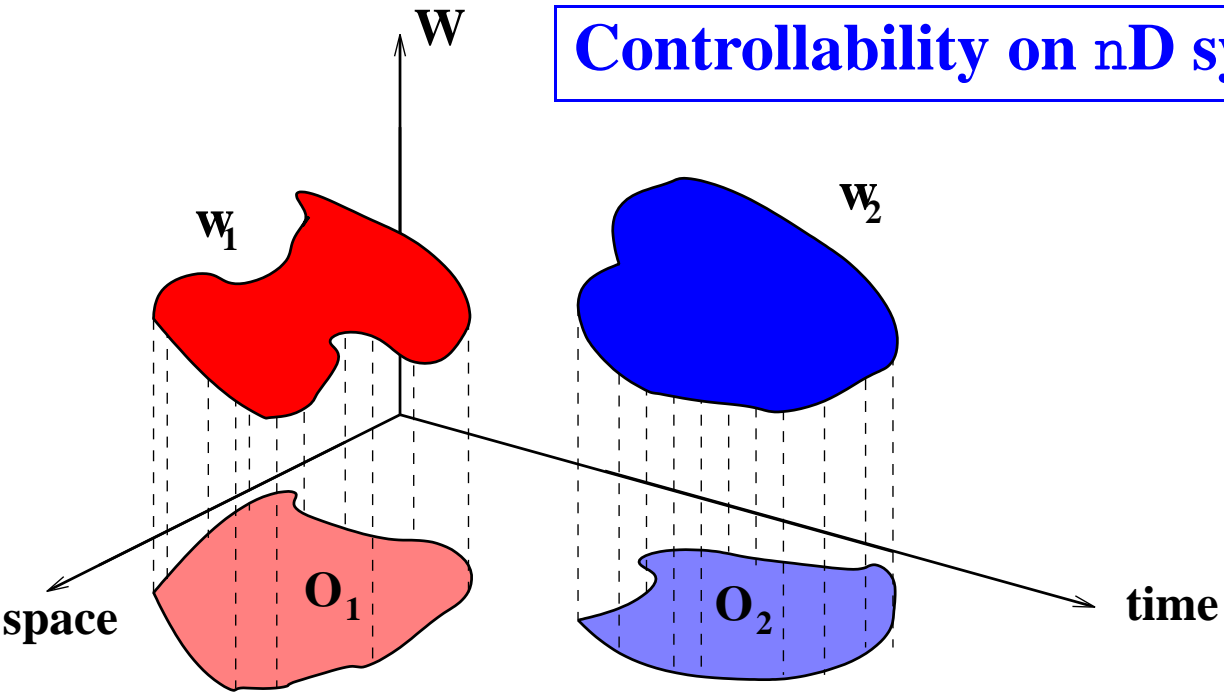
Eliminate \vec{B} from Maxwell's equations \rightsquigarrow

$$\begin{aligned}\nabla \cdot \vec{E} &= \frac{1}{\epsilon_0} \rho, \\ \epsilon_0 \frac{\partial}{\partial t} \nabla \cdot \vec{E} + \nabla \cdot \vec{j} &= 0, \\ \epsilon_0 \frac{\partial^2}{\partial t^2} \vec{E} + \epsilon_0 c^2 \nabla \times \nabla \times \vec{E} + \frac{\partial}{\partial t} \vec{j} &= 0.\end{aligned}$$

Controllability on nD systems

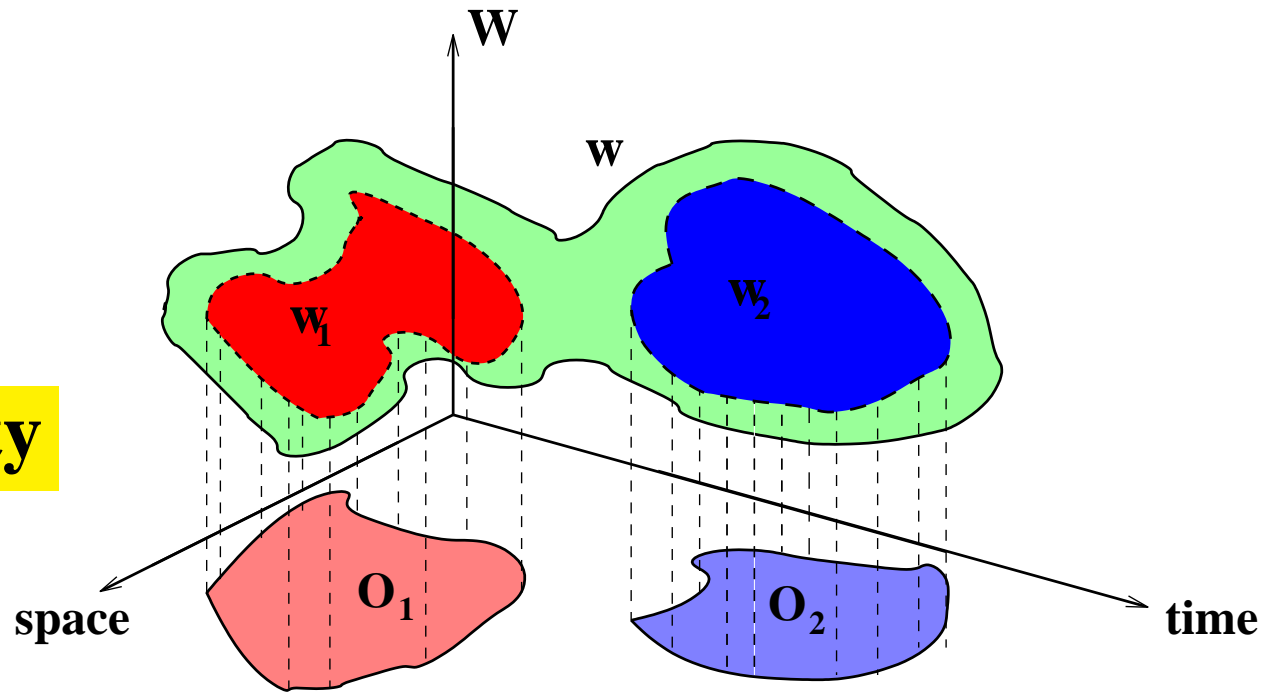


Controllability on nD systems



Controllability

:= Patchability



Controllability on nD systems

$\mathfrak{B} \in \mathcal{L}_n^w$ controllable if and only if it has a repr.

$$w = M \left(\frac{\partial}{\partial x_1}, \dots, \frac{\partial}{\partial x_n} \right) \ell$$

$$\mathfrak{B} = \text{image} \left(M \left(\frac{\partial}{\partial x_1}, \dots, \frac{\partial}{\partial x_n} \right) \right)$$

Is an image a kernel? Always! \Leftarrow Elimination th'm

Is a kernel an image? Iff the kernel is controllable!

Controllability on nD systems

$\mathfrak{B} \in \mathcal{L}_n^w$ controllable if and only if it has a repr.

$$w = M \left(\frac{\partial}{\partial x_1}, \dots, \frac{\partial}{\partial x_n} \right) \ell$$

$$\mathfrak{B} = \text{image} \left(M \left(\frac{\partial}{\partial x_1}, \dots, \frac{\partial}{\partial x_n} \right) \right)$$

But, for $n > 1$, this image may not be **observable**.

Images may require **hidden variables**.

Are EM fields controllable ?

Are EM fields controllable ?

The following eq'ns in

scalar potential $\phi : \mathbb{R} \times \mathbb{R}^3 \rightarrow \mathbb{R}$

vector potential $\vec{A} : \mathbb{R} \times \mathbb{R}^3 \rightarrow \mathbb{R}^3$

generate exactly the solutions to MEs:

$$\vec{E} = -\frac{\partial}{\partial t}\vec{A} - \nabla\phi,$$

$$\vec{B} = \nabla \times \vec{A},$$

$$\vec{j} = \epsilon_0 \frac{\partial^2}{\partial t^2} \vec{A} - \epsilon_0 c^2 \nabla^2 \vec{A} + \epsilon_0 c^2 \nabla (\nabla \cdot \vec{A}) + \epsilon_0 \frac{\partial}{\partial t} \nabla \phi,$$

$$\rho = -\epsilon_0 \frac{\partial}{\partial t} \nabla \cdot \vec{A} - \epsilon_0 \nabla^2 \phi.$$

Are EM fields controllable ?

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$$\vec{B} = \nabla \times \vec{A},$$

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$$\rho = -\varepsilon_0 \frac{\partial}{\partial t} \nabla \cdot \vec{A} - \varepsilon_0 \nabla^2 \phi.$$

Proves controllability of EM fields.

Not observable, cannot be !

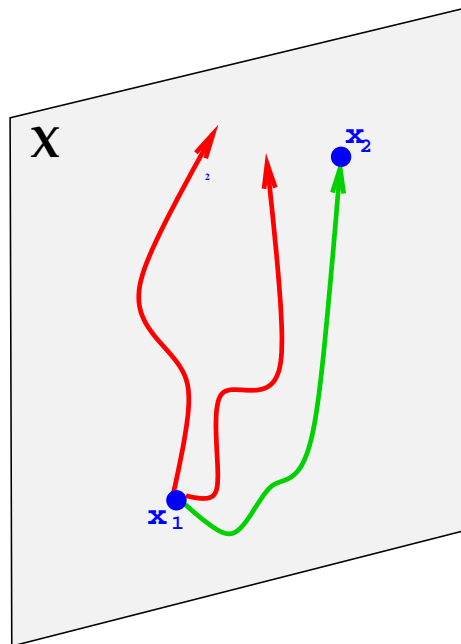
controllability $\Leftrightarrow \exists$ potential!

Control

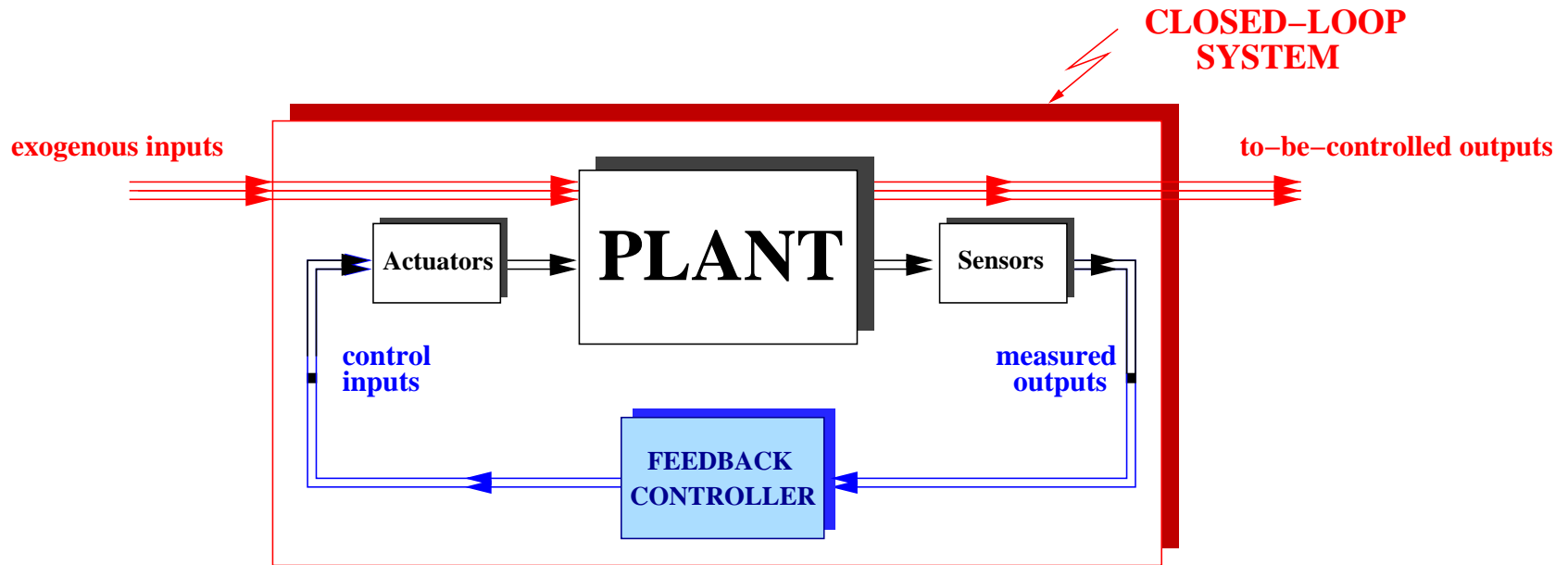
Path planning

$$\frac{d}{dt}x = f(x, u)$$

Choose time-function $u(\cdot) : [0, T] \rightarrow \mathbb{U}$ so as to achieve (optimal) state transfer. **‘open loop control’**



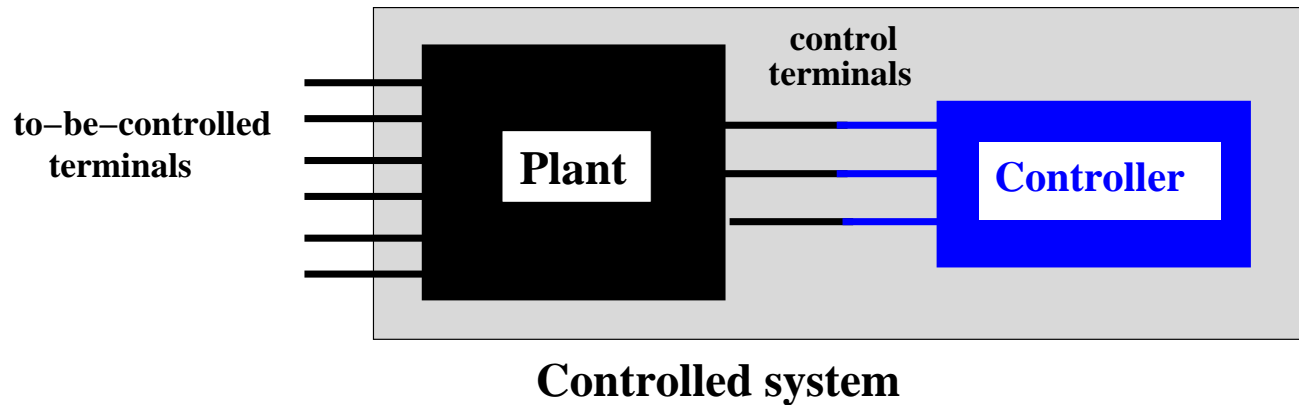
Decision making



Choose **map from sensor outputs to actuator inputs** so as to achieve good (optimal) performance.

‘feedback control’
‘closed loop control’
‘intelligent control’

Embedded systems



Choose **controller** so as to achieve good (optimal) performance of the interconnected system

‘control as interconnection’
‘integrated system design’

Look back

Behavioral systems

- **Gets the physics right**

Behavioral systems

- Gets the physics right
- Deals faithfully with interconnections: variable sharing

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- **Views control as interconnection**
- **Advantages in SYSID, etc.**
- **Far easier pedagogically**
- **...**

Details & copies of frames are available from/at

Jan.Willems@esat.kuleuven.be

<http://www.esat.kuleuven.be/~jwillems>

Thank you

Thank you

Thank you

Thank you

Thank you

Thank you

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