# **DSP-CIS**

Part-II: Filter Design and Implementation

Chapter-4: Filter Design

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# Filter Design Process

• Step-1 : Define filter specs

Pass-band, stop-band, optimization criterion,...

• Step-2: Derive optimal transfer function

FIR or IIR filter design

**Chapter-4** 

• Step-3: Filter realization (block scheme/flow graph)

Direct form realizations, lattice realizations,... Chapter-5

• <u>Step-4</u>: Filter implementation (software/hardware)

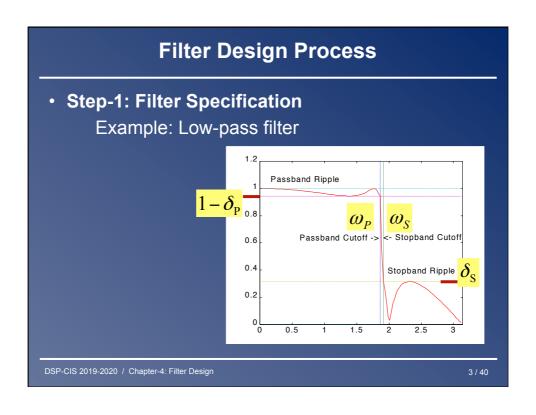
Finite word-length issues, ...

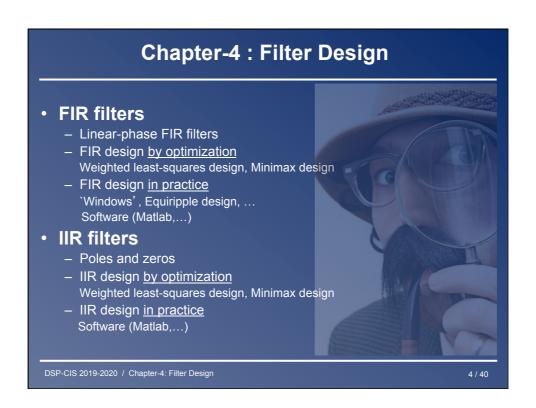
**Chapter-6** 

Question: implemented filter = designed filter?

'You can't always get what you want' -Jagger/Richards (?)

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#### **FIR Filters**

FIR filter = finite impulse response filter

$$H(z) = \frac{B(z)}{z^{L}} = b_0 + b_1 z^{-1} + \dots + b_L z^{-L}$$

- L poles at the origin z=0 (hence guaranteed stability)
- · L zeros (zeros of B(z)), 'all zero' filters
- · Corresponds to difference equation

$$y[k] = b_0.u[k] + b_1.u[k-1] + ... + b_L.u[k-L]$$

- Hence also known as 'moving average filters' (MA)
- Impulse response

$$h[0] = b_0, h[1] = b_1, ..., h[L] = b_L, h[L+1] = 0,...$$

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• Non-causal zero-phase filters :

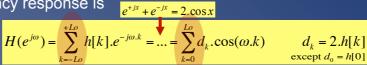
Example: symmetric impulse response (length 2.L<sub>0</sub>+1)

$$h[-L_{\circ}],....h[-1], h[0], h[1],...,h[L_{\circ}]$$

 $h[k]=h[-k], k=1..L_0$ 



Frequency response is



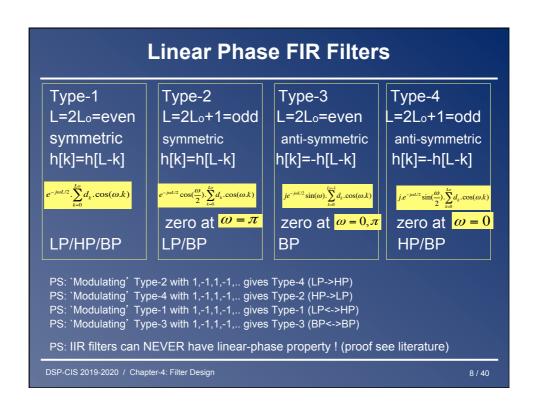
2Lo+1 terms

Lo+1 terms

i.e. real-valued (=zero-phase) transfer function

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#### **Linear Phase FIR Filters** Causal linear-phase filters = non-causal zero-phase + delay Example: symmetric impulse response & L even h[0],h[1],....,h[L] L=2.L<sub>o</sub> h[k]=h[L-k], k=0..L01 Frequency response is $H(e^{j\omega}) = \sum_{k=0}^{L} h[k] \cdot e^{-j\omega \cdot k} = \dots = e^{-j\omega \cdot Lo} \cdot \sum_{k=0}^{Lo} d_k \cdot \cos(\omega \cdot k)$ $d_k = 2.h[k + Lo]$ except $d_0 = h[Lo]$ = i.e. causal implementation of zero phase filter, by ← phase is linear function introducing delay of frequency DSP-CIS 2019-2020 / Chapter-4: Filter Design 7 / 40



- (I) Weighted Least Squares Design:
- Select one of the basic forms that yield linear phase e.g. Type-1  $H(e^{j\omega}) = e^{-j\omega L/2} \cdot \sum_{k=0}^{Lo} d_k \cdot \cos(\omega . k) = e^{-j\omega L/2} \cdot \left| H(\omega) \right|^{\Delta} = e^{-j\omega L/2} \cdot G(\omega)$
- Specify desired frequency response (LP,HP,BP,...)  $H_d(\omega) = e^{-j\omega L/2}.G_d(\omega)$
- Optimization criterion is

$$\min_{d_0,\dots,d_{L_o}} \int_{-\pi}^{+\pi} W(\omega) \left| H(e^{j\omega}) - H_d(\omega) \right|^2 d\omega = \min_{d_0,\dots,d_{L_o}} \int_{-\pi}^{+\pi} W(\omega) \left| G(\omega) - G_d(\omega) \right|^2 d\omega$$

where  $\overline{W(\omega) \ge 0}$  is a weighting function

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# FIR Filter Design by Optimization

· This is 'Quadratic Optimization' problem

$$\min_{x} \left\{ \int_{-\pi}^{\pi} W(\omega) \left| c^{T}(\omega) \cdot \begin{bmatrix} d_{0} \\ \vdots \\ d_{Lo} \end{bmatrix} - G_{d}(\omega) \right|^{2} d\omega \right\} = \min_{x} \underbrace{\{x^{T} \cdot Q \cdot x - 2x^{T} \cdot p + \mu\}}_{F(d_{0}, \dots, d_{Lo})}$$

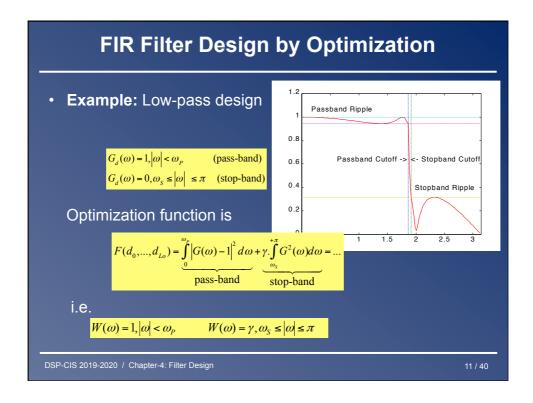
$$x^{T} = \begin{bmatrix} d_{0} & d_{1} & \dots & d_{Lo} \end{bmatrix} \qquad c^{T}(\omega) = \begin{bmatrix} 1 & \cos(\omega) & \dots & \cos(Lo.\omega) \end{bmatrix}$$

$$Q = \int_{-\pi}^{\pi} W(\omega).c(\omega).c^{T}(\omega)d\omega \qquad p = \int_{-\pi}^{\pi} W(\omega).G_{d}(\omega).c(\omega)d\omega$$

u = ...

... with solution  $x_{OPT} = Q^{-1} p$ 

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• A simpler problem is obtained by replacing the F(..) by...

$$\underline{F}(d_0,...,d_{Lo}) = \sum_i W(\omega_i) \cdot \left| G(\omega_i) - G_d(\omega_i) \right|^2$$

where the wi's are a set of sample frequencies

This leads to an equivalent ('discretized') quadratic optimization function:

$$\underline{F}(d_0, ..., d_{Lo}) = \sum_{i} W(\omega_i) \left\{ c^T(\omega_i) . \begin{bmatrix} d_0 \\ \vdots \\ d_{Lo} \end{bmatrix} - G_d(\omega_i) \right\}^2 = x^T . \underline{Q} . x - 2x^T . \underline{p} + \underline{\mu}$$

$$\underline{Q} = \sum_{i} W(\omega_{i}).c(\omega_{i}).c^{T}(\omega_{i}), \qquad \underline{p} = \sum_{i} W(\omega_{i}).G_{d}(\omega_{i}).c(\omega_{i}), \qquad \underline{\mu} = \dots$$

 $x_{OPT} = \underline{Q}^{-1} \cdot \underline{p}$ 

Compare to p.10



+++ Simple

--- Unpredictable behavior in between sample freqs.

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• This is often supplemented with additional constraints, e.g. for pass-band and stop-band ripple control:

$$\begin{split} \left|G(\omega_{P,j})-1\right| &\leq \delta_{\mathbb{P}}, \quad \text{for pass-band freqs. } \omega_{P,1},\omega_{P,2},\dots \quad (\delta_{\mathbb{P}} \text{ is pass-band ripple}) \\ \left|G(\omega_{S,j})\right| &\leq \delta_{\mathbb{S}}, \quad \text{for stop-band freqs. } \omega_{S,1},\omega_{S,2},\dots \quad (\delta_{\mathbb{S}} \text{ is stop-band ripple}) \end{split}$$

· The resulting optimization problem is :

minimize : 
$$\underline{\underline{F}(d_0,...,d_{Lo})} = ...$$
 (=quadratic function) 
$$x^T = \left[ \begin{array}{cccc} d_0 & d_1 & ... & d_{Lo} \end{array} \right]$$

subject to  $G_p.x \le b_p$  (=pas

 $G_p.x \le b_p$  (=pass-band constraints)  $G_s.x \le b_s$  (=stop-band constraints)

= `Quadratic Programming' problem

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# **FIR Filter Design by Optimization**

# (II) `Minimax' Design:

- Select one of the basic forms that yield linear phase e.g. Type-1  $\frac{L_0}{H(e^{j\omega}) = e^{-j\omega L/2}} \cdot \sum_{k=0}^{L_0} d_k \cdot \cos(\omega \cdot k) = e^{-j\omega N/2} \cdot G(\omega)$
- Specify desired frequency response (LP,HP,BP,...)

$$H_d(\omega) = e^{-j\omega L/2} \cdot G_d(\omega)$$

Optimization criterion is

$$\begin{aligned} & \min_{d_0,\dots,d_{Lo}} \max_{-\pi \leq \omega \leq \pi} W(\omega) \Big| H(e^{j\omega}) - H_d(\omega) \Big|^2 = \min_{d_0,\dots,d_{Lo}} \max_{-\pi \leq \omega \leq \pi} W(\omega) \Big| G(e^{j\omega}) - G_d(\omega) \Big|^2 \\ & \text{where} \quad & \underline{W(\omega) \geq 0} \quad \text{is a weighting function} \end{aligned}$$

Leads to `Semi-Definite Programming' (SDP) problem, for which efficient interior-point algorithms & software are available.

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- Conclusion:
  - (I) Weighted least squares design
  - (II) Minimax design provide general `framework' , procedures to translate filter design problems into standard optimization problems
- In practice (and in textbooks):

Emphasis on specific (ad-hoc) procedures:

- Filter design based on 'windows'
- Equiripple design

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# FIR Filter Design using 'Windows'

### **Example: Low-pass filter design**

• Ideal low-pass filter is

$$H_{d}(\omega) = \begin{cases} 1 & |\omega| < \omega_{C} \\ 0 & \omega_{C} \prec |\omega| < \pi \end{cases}$$

Hence ideal time-domain impulse response is (non-causal zero-phase)

$$h_d[k] = \frac{1}{2\pi} \int_{-\pi}^{+\pi} H_d(e^{j\omega}) e^{j\omega k} d\omega = \dots = \alpha \cdot \frac{\sin(\omega_c k)}{\omega_c k} \qquad -\infty < k < \infty$$

• Truncate hd[k] to L+1 samples (L even):

$$h[k] = \begin{cases} h_d[k] & -L/2 < k < L/2 \\ 0 & \text{otherwise} \end{cases}$$

· Add delay to turn into causal filter

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## FIR Filter Design using 'Windows'

#### **Example: Low-pass filter design (continued)**

- PS: It can be shown (use Parceval's theorem) that the filter obtained by such time-domain truncation is also obtained by using a weighted least-squares design procedure with the given Hd (+linear phase) and weighting function  $W(\omega) = 1$
- Truncation corresponds to applying a `rectangular window' :

$$h[k] = h_d[k].w[k]$$

$$w[k] = \begin{cases} 1 & -L/2 < k < L/2 \\ 0 & \text{otherwise} \end{cases}$$

- +++ Simple procedure (also for HP,BP,...)
- - Truncation in time-domain results in `Gibbs effect' in frequency domain, i.e. large ripple in pass-band and stop-band (at band edge discontinuity), which cannot be reduced by increasing the filter order L.

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# FIR Filter Design using 'Windows'

### Remedy: Apply other window functions...

• Time-domain multiplication with a window function w[k] corresponds to frequency domain convolution with W(z):

$$h[k] = h_d[k].w[k]$$

$$H(z) = H_d(z)*W(z)$$

- Candidate windows: Han, Hamming, Blackman, Kaiser,.... (see textbooks, see DSP-I)
- Window choice/design = trade-off between side-lobe levels (define peak pass-/stop-band ripple) and width main-lobe (defines transition bandwidth), see examples p.25-28

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### FIR Equiripple Design

· Starting point is minimax criterion, e.g.

$$\min_{d_0,\dots,d_{L^o}} \max_{0 \leq \omega \leq \pi} W(\omega). \left| G(\omega) - G_d(\omega) \right| = \min_{d_0,\dots,d_{L^o}} \max_{0 \leq \omega \leq \pi} \left| E(\omega) \right|$$

Based on theory of Chebyshev approximation and the `alternation theorem', which (roughly) states that the optimal d's are such that the `max' (maximum weighted approximation error) is obtained at L₀+2 extremal frequencies...

$$\max_{0 \le \omega \le \pi} |E(\omega)| = |E(\omega_i)|$$
 for  $i = 1,..,Lo + 2$ 

...that hence will exhibit the same maximum ripple ('equiripple')

- Iterative procedure for computing extremal frequencies, etc. (<u>Remez</u> exchange algorithm, <u>Parks-McClellan</u> algorithm)
- · Very flexible, etc., available in many software packages
- Details omitted here (see textbooks)

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# FIR Filter Design Software

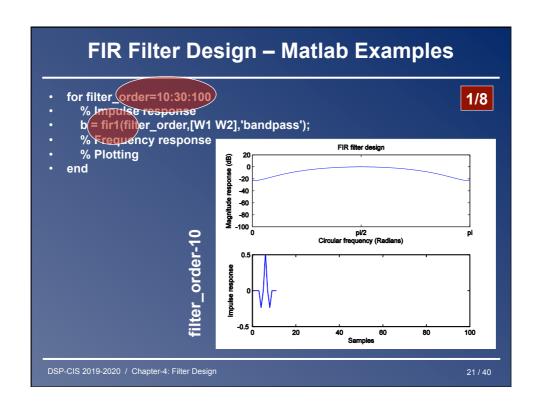
- FIR Filter design abundantly available in commercial software
- Matlab:

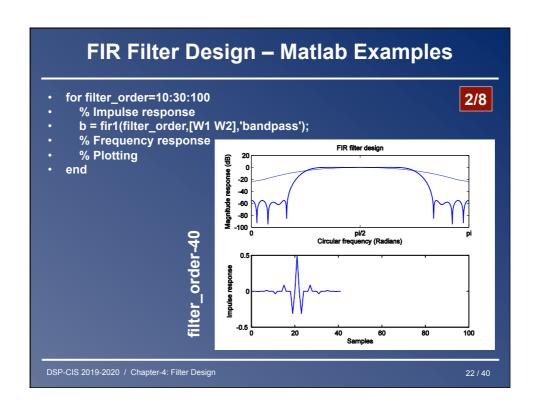
b=fir1(L,Wn,type,window), windowed linear-phase FIR design, L is filter order, Wn defines band-edges, type is `high', `stop',...

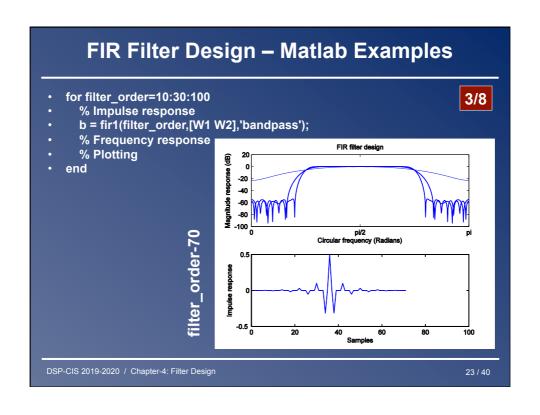
b=fir2(L,f,m,window), windowed FIR design based on inverse Fourier transform with frequency points f and corresponding magnitude response m

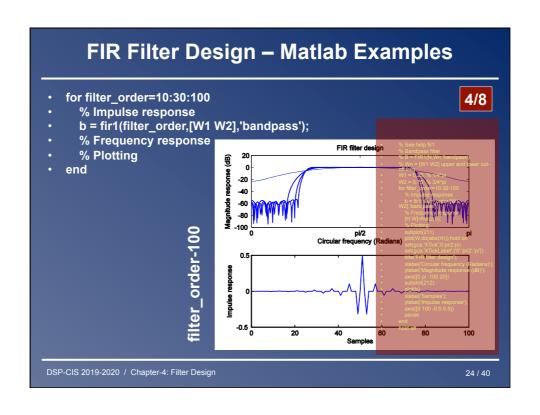
b=remez(L,f,m), equiripple linear-phase FIR design with Parks-McClellan (Remez exchange) algorithm

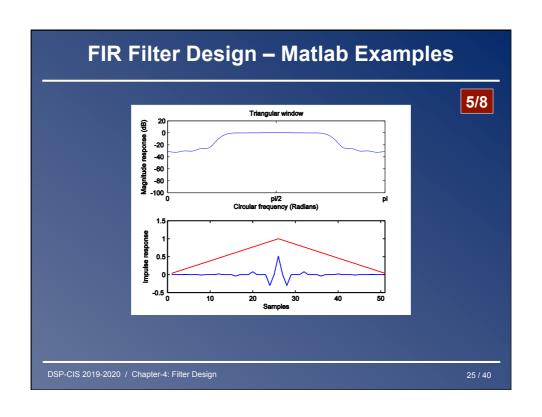
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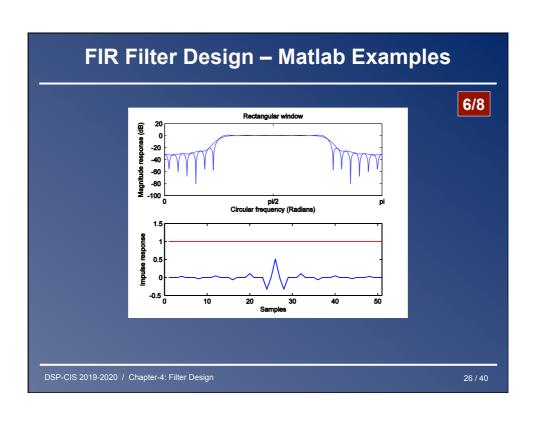


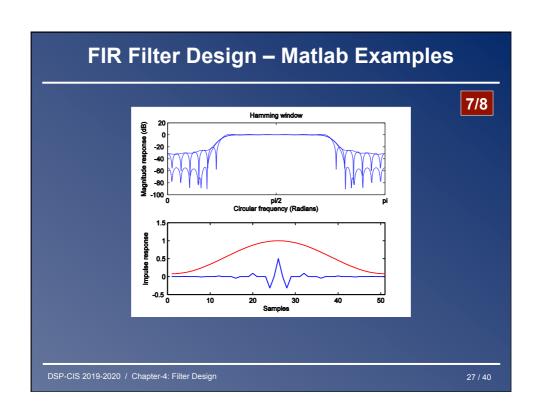


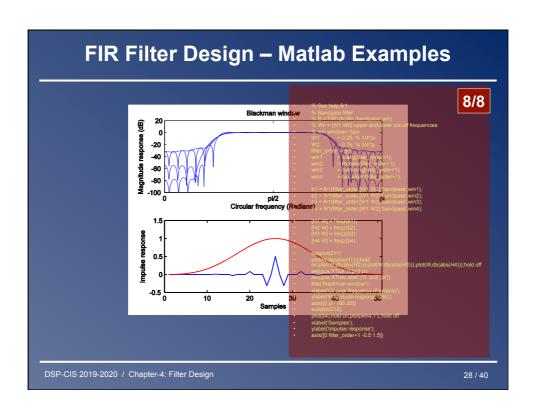












#### **IIR filters**

#### Rational transfer function:

$$H(z) = \frac{B(z)}{A(z)} = \frac{b_0 z^L + b_1 z^{L-1} + \dots + b_L}{z^L + a_1 z^{L-1} + \dots + a_L} = \frac{b_0 + b_1 z^{-1} + \dots + b_L z^{-L}}{1 + a_1 z^{-1} + \dots + a_L z^{-L}}$$

L poles (zeros of A(z)), L zeros (zeros of B(z))

- · Infinitely long impulse response
- · Stable iff poles lie inside the unit circle
- · Corresponds to difference equation

$$y[k] + a_1 \cdot y[k-1] + \dots + a_L \cdot y[k-L] = b_0 \cdot u[k] + b_1 \cdot u[k-1] + \dots + b_L \cdot u[k-L]$$

$$y[k] = \underbrace{b_0.u[k] + b_1.u[k-1] + \dots + b_L.u[k-L]}_{MA'} \underbrace{-a_1.y[k-1] - \dots - a_L.y[k-L]}_{AR'}$$

= also known as `ARMA' (autoregressive-moving average)

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# **IIR Filter Design**

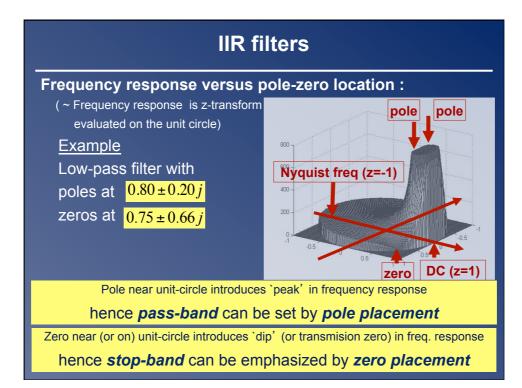


- · Low-order filters can produce sharp frequency response
- Low computational cost (cfr. difference equation p.29)

-

- · Design more difficult
- · Stability should be checked/guaranteed
- Phase response not easily controlled (e.g. no linear-phase IIR filters)
- Coefficient sensitivity, quantization noise, etc. can be a problem (see Chapter-6)

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## (I) Weighted Least Squares Design:

· IIR filter transfer function is

$$H(z) = \frac{B(z)}{A(z)} = \frac{b_0 + b_1 z^{-1} + \dots + b_L z^{-L}}{1 + a_1 z^{-1} + \dots + a_L z^{-L}}$$

Specify desired frequency response (LP,HP,BP,...)

$$H_d(\omega)$$

· Optimization criterion is

$$\min_{b_0,\dots,b_L,a_1,\dots,a_L} \int_{-\pi}^{+\pi} W(\omega) \left| H(e^{j\omega}) - H_d(\omega) \right|^2 d\omega$$

$$F(b_0,\dots,b_L,a_1,\dots,a_L)$$

where  $W(\omega) \ge 0$  is a weighting function

• Stability constraint :  $A(z) \neq 0, |z| \geq 1$ 

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#### (II) 'Minimax' Design:

· IIR filter transfer function is

$$H(z) = \frac{B(z)}{A(z)} = \frac{b_0 + b_1 z^{-1} + \dots + b_L z^{-L}}{1 + a_1 z^{-1} + \dots + a_L z^{-L}}$$

• Specify desired frequency response (LP,HP,BP,...)

$$H_d(\omega)$$

Optimization criterion is

$$\min_{b_0,\dots,b_L,a_1,\dots,a_L} \max_{0 \le \omega \le \pi} W(\omega). \left| H(e^{j\omega}) - H_d(\omega) \right|$$

where  $W(\omega) \ge 0$  is a weighting function

• Stability constraint:

$$A(z) \neq 0, |z| \ge 1$$

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# **IIR Filter Design by Optimization**

These optimization problems are significantly more difficult than those for the FIR design case...:

- <u>Problem-1</u>: Presence of denominator polynomial leads to non-linear/non-quadratic optimization
- <u>Problem-2</u>: Stability constraint
   (zeros of a high-order polynomial are related to the its coefficients in a highly non-linear manner)
  - Solutions based on alternative stability constraints, that
     e.g. are affine functions of the filter coefficients, etc...
  - Topic of ongoing research, details omitted here

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- Conclusion:
  - (I) Weighted least squares design
  - (II) Minimax design provide general `framework', procedures to translate filter design problems into ``standard'' optimization problems
- In practice (and in textbooks):

Emphasis on specific (ad-hoc) procedures:

- IIR filter design based *analog filter design* (Butterworth, Chebyshev, elliptic,...) and *analog->digital conversion*
- IIR filter design by *modeling* = direct z-domain design (Pade approximation, Prony, etc., not addressed here)

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### **IIR Filter Design Software**

- IIR filter design considerably more complicated than FIR design (stability, phase response, etc..)
- (Fortunately) IIR Filter design abundantly available in commercial software
- Matlab:

[b,a]=butter/cheby1/cheby2/ellip(L,...,Wn),

IIR LP/HP/BP/BS design based on analog prototypes, pre-warping, bilinear transform, ...

immediately gives H(z) ☺

analog prototypes, transforms, ... can also be called individually filter order estimation tool

etc...

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